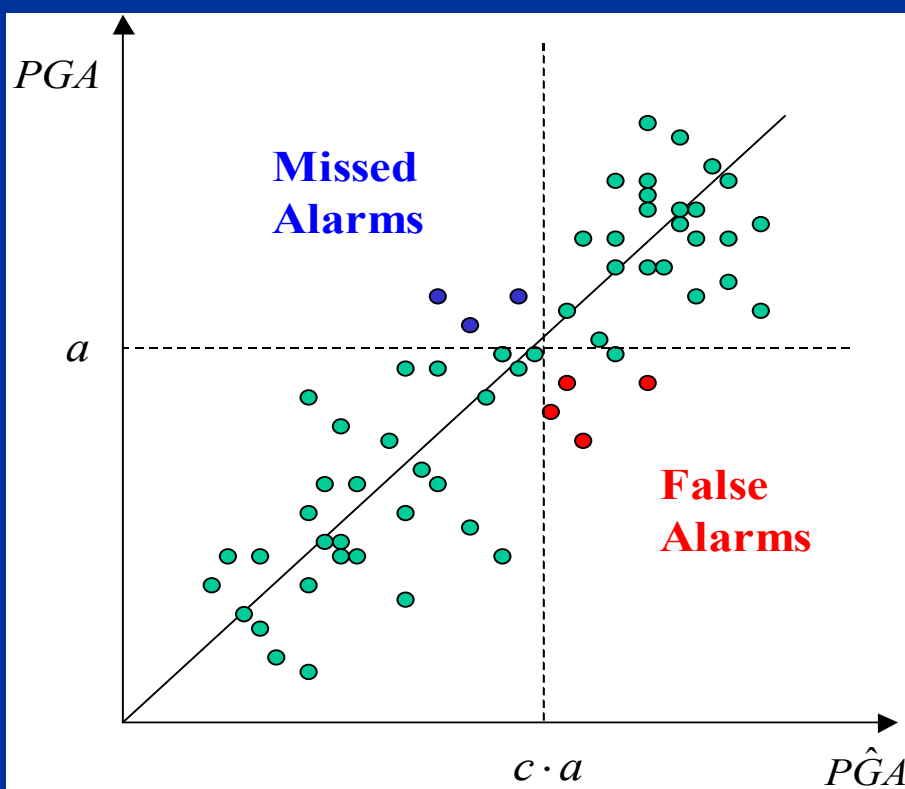




Università degli Studi di Napoli Federico II

Seismic Early Warning Systems: Procedure for Automated Decision Making

Dottorato di Ricerca in Rischio Sismico



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*“Nel Mondo nulla di grande
è stato fatto senza passione”*

Hegel

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Seismic early warning systems: procedure for automated decision making

Veronica Francesca Grasso

Chapter 1

1. Introduction

The high social and economical relevance of the seismic risk associated with the high vulnerability of urbanized areas has become evident in recent years due to severe losses as a consequence of catastrophic seismic events. A detailed analysis of structural damages and economic losses due to catastrophic events underlines the strong necessity of social, political and scientific cooperation for disaster prevention. Historical lessons are of some help to point out the evidence that timely warning could mitigate the effects of natural disasters.

In the recent Asian tsunami disaster occurring on 26 December 2004, thousands of lives could have been saved if a preventive alarm and prediction had been effective, in terms of warning time and reliability, to warn the people about the coming event. At the moment the earthquake occurred in Sumatra, alarm messages could have been sent to the endangered areas. By the time the tsunami arrived, many people might have been able to escape from the coastal areas, reaching higher locations. In addition, the availability of inundation and damage maps in the few minutes after the seismic event could have saved many other people by effective and immediate emergency aid, if an emergency response system was in place.

Early warning technologies are a key component for an effective and efficient protection from catastrophic natural disasters, seconds before, during and after the event (Wieland, 2001).

Early warning systems (EWS) have been recently developed as an innovative technology for natural risk mitigation that could be applied to all natural disasters, although the attention here is focused on seismic risk mitigation. Effective early warning technologies for earthquakes are much more challenging to develop because warning times range from only a few seconds to a minute or so (Allen and Kanamori, 2003). In areas close to faults, where seismic EWS represent a mandatory necessity, only tens of seconds of warning are available. Such short warning time means that to be effective, a seismic EWS must depend on automated procedures, including those for decision making about whether to activate mitigation measures; the time is too short to require human intervention when the event is first detected. As a result of the automation, careful attention must be

paid to the design of the local seismic EWS for each critical facility; in particular, a means of controlling the trade-off between false alarms and missed alarms is desirable.

Although early warning technologies have been developed to provide natural hazard mitigation for many types of hazards, attention here is focused on seismic risk mitigation because the technologies for this application are not yet fully developed.

1.1. Considerations and Road Map

The main goal of EWS is the reduction of loss of lives and mitigation of structural damage and economic loss. EWS impact or effectiveness is strictly dependent on the warning time available and the quality of the information provided that influences and constrains the utilization of the information. Timeliness and reliability are contradictory design requirements.

Solving the trade-off between timeliness and reliability is often a problem with not a uniquely determined solution. As from the state-of-art analysis accuracy of estimates is of general interest and represents one of the main goals for existing EWS improvements (as Iglesias et al. 2005, Veneziano et al., 1998).

The benefits of an EWS for earthquakes are often not fulfilled due to limitations that depend on the amount of warning time and accuracy of the prediction. These parameters strongly influence EWS impact and effectiveness on seismic risk reduction. Suppose that the EWS works by setting an alarm if a critical shaking intensity threshold is predicted to be exceeded at a site, where the choice of critical threshold depends on the vulnerability of the system to be protected at the site. Assuming that the warning time provided by the EWS is sufficient for activation of the mitigation measure, then based on the predictions from the first few seconds of P-wave observation, a decision has to be made of whether to activate the alarm or not. Since prediction is uncertain in making this decision we may committ two kinds of errors, false alarms and missed alarms. As a consequence a key element of an EWS is a better understanding of the parameters that play a fundamental role in this uncertainty. As a result performance-based approach to EWS design and decision models is a mandatory necessity.

A frame-work for the uncertainty estimation in real-time is presented (Chapter 4), representing a fundamental information to be sent to the user. In addition is presented, in Chapter 3-6, a performance-based design approach to EWS for a rational warning threshold setting based on the evaluation of the consequences expressed in costs and benefits (that may be monetary or loss of lives). A decision model (Chapter 7) is then presented for making a decision in a real-time scenario based on the expected consequences and savings coming from the decision itself.

Chapter 2

2. EWS: State-of-art

In order to mitigate the seismic risk, different approaches are possible such as seismic design of structures or strengthening of existing buildings. Quite recently a more innovative technology has been developed, based on “early warning systems” (EWS).

To introduce the EWSs, consider that, dealing with seismic risk mitigation, different approaches can be considered related to the phases of an earthquake event (Wieland 2001):

1. Prevention during the years before an earthquake. Related measures: seismic design and strengthening of buildings and installations; preparation of emergency plans, to conduct programs for earthquake preparedness of population, installation of earthquake early warning, seismic alarm and earthquake rapid response systems. Please notice that for financial reasons, not all the buildings can be strengthened and, therefore, a scale of priority is needed .
2. Early Warning Systems are represented by the measures that can be carried out from the moment in which a seismic event is triggered, with sufficient reliability, in a given place. These measures, for prevention or emergency, can be classified considering the time of warning available: as examples, evacuation of buildings, shut-down of critical systems (nuclear and chemical reactors), stop of high-speed trains.

Wieland (2000) evidenced the benefits in different fields as a consequence of the implementation of EWS. A qualitative analysis shows that earthquake early warning, seismic alarm and earthquake rapid response systems can be effective for seismic risk mitigation, in every phase of the seismic event. Social preparedness associated with a sufficient warning time could prevent loss of lives, on the other hand few seconds of warning may give the possibility to put into a safer position critical facilities and transportation systems, and to improve rescue operations. Within seconds after an earthquake, the information provided by EWS could be used to produce damage and loss maps based on the ground shaking intensity and could be the basis for more efficient emergency response and rescue operations. More recently an interesting application of EWS is emerging for the protection of strategic buildings (e.g. hospitals, public buildings, buildings of hystorical interest), by the activation of structural control systems.

The first idea of an earthquake EWS has been developed by Cooper in 1868 for San Francisco, California. Cooper proposed to create a network of seismic detectors in the epicentral area. An electric signal, in case of an earthquake event, would be sent by telegraph to San Francisco, where

the ring of a bell, situated in the City Hall, would alert the population. Unfortunately, Cooper's idea was never realized and only 100 years later the first early warning system has become effective. In 1985, Heaton proposed a seismic alert network for South California. For the earthquake of Loma Prieta, in 1989, Bakun et al. implemented a seismic EWS.

The principle on which EWSs are based can be addressed to the characteristic of seismic waves that travel with a velocity that is less than electromagnetic signals transmitted by telephone or radio, used to transmit the seismic informations about the incoming event (which travel at a velocity of about 300000 Km/s). In addition, seismic waves can be identified as compression waves (primary waves, P-waves) and shear waves (secondary waves, S-waves); in particular P-waves are characterized by a velocity that is almost two times the travel velocity of S-waves, that cause structural damage. The time interval from the arrival of P-waves and the S-waves may be utilized to activate security measures. The feasible warning time is evaluated by Eqs. 2.1, 2.2 :

$$T_w = T_s - T_r \quad 2.1$$

$$T_r = T_d + T_{pr} \quad 2.2$$

where T_r is the reporting time constituted by the time T_d needed by the system to trigger and record a sufficient length of waveforms and the time T_{pr} to process the data, T_s is the S wave travel time and finally, T_w is the early warning time, as synthetized in Fig. 2.1.

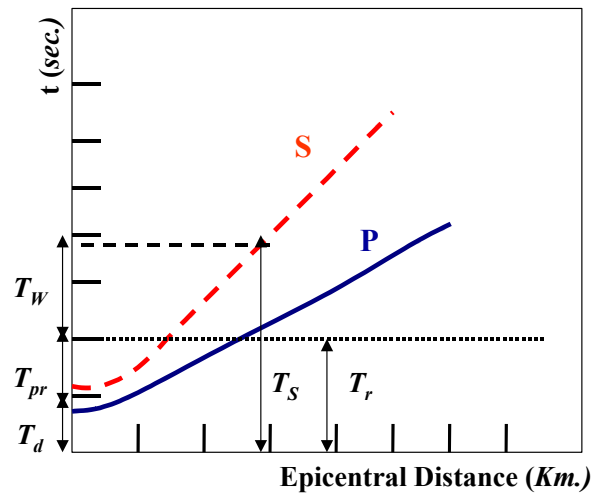


Figure 2.1: P and S-waves arrival time as a function of distance from an earthquake

2.1. Early Warning Systems

EWS is constituted by: a distributed network of seismometers and strong motion recording instruments; real-time data communications to a central data processing; central processing facility; warning information packet and area wide broadcasting system; warning information receivers. The

seismic network could be distributed in the epicentral area (i.e. Mexico City and Bucharest EWS), or localized around the area to protect (i.e. Ignalina power plant EWS, Wieland 2000), if the epicenter is unknown. In the case of uncertain source zone a virtual subnetwork approach is possible (Wu and Teng, 2002).

The network is composed by remote sensing stations that transmit in real-time to the central processor that provides to calculate in real-time seismic parameters such as location, origin time, magnitude. If the threshold is exceeded, a warning signal is transmitted over an area-wide transmitter. The message contains informations of the incoming event. A dedicated receiver, part of the user's system, collects and processes the data, in order to activate security measures (automatic or manual), when the user's facility tolerances are exceeded. The central unit is dedicated to receive signals transmitted by the stations and the central processor provides a real-time analysis. As the event evolves, more data are available in order to confirm and increase the accuracy of the informations processed starting from the incoming signals. The location of the epicenter, magnitude, maximum ground acceleration, spectrum response analysis, damage maps are the informations that can be provided by EWS, as from the state-of-art review.

The data that will be later processed by the central unit, are limited to the first seconds of registration of a limited number of sensors (i.e. in (Allen and Kanamori, 2003) the number of sensors is 10, and 7 is the number proposed in (Wu and Teng, 2002)). The definition of the time of observation and the number of sensors of interest is obtained by minimizing the error of estimate and maximizing the warning time feasible. The data are processed and the estimate of the seismic parameters (as epicentral distance and magnitude) are defined by a predictive model. The parameters of structural interest, as peak ground acceleration (PGA) or spectral acceleration (Sa), are defined by an attenuation model, taking into account the distance from the structure and the epicenter and the geotechnical characteristics of the soils invested by the seismic waves. Reliability data associated to information relative to the seismic parameters of the incoming earthquake could be a fundamental tool to prevent false alarms; the decision is demanded, in this way, to the user itself, related to the level of reliability and to the effects of false alarms. Note that the parameter of interest for a facility could also be taken as some critical engineering demand parameter (EDP) as in Chapter 4, such as interstory drift in a building or floor acceleration at the location of vulnerable equipment or even economic loss (Chapter 8).

2.2. Existing EWS applications

Early warning refers to real-time seismology in which seismic data are collected and analysed in real-time for an early warning or post-event utilization of this information.

For early warning two approaches are possible (Kanamori 2004):

- Regional warning
- On-site (or site-specific) warning

Traditional approaches refer to the regional method that consists in estimating location and magnitude of the event and predicting ground motion at other sites. The on-site approach is related to predicting the ground shaking at the site is not necessary to locate the event and predict the magnitude. While the first approach is more reliable the second is much faster.

The second approach could provide useful early warning for sites close to the epicenter.

This approach requires a deep understanding of earthquake rupture and physics in order to estimate the nature of the evolving rupture only from the first observation.

The traditional approach (first one) has been already applied for Japan, Mexico City, Taiwan and Turkey (Erdik et al., 2003; Boese et al., 2004), while the second approach has been done by Kanamori (2004), Wu and Kanamori (2004).

The most important and effective EWS application is in Japan developed in the 1960's by the Japanese Railway to avoid trains derailment in case of heavy ground shaking (Nakamura, 1988).

EWS has been applied to the high velocity Shinkansen railway line, based on the P-wave detection and the installation of the stations near the epicentral zone far from the railroad, providing time for an early warning.

Ordinary alarm seismometers were installed along the coast line at the Tohoku area in 1984 to complete the early warning system and this system can control the train operation before the main shock reaches the railroad. An existing system is present along the Shinkansen line, composed by ordinary alarm seismometers that had been installed in 1965 every 20-25 km. The system issues an alarm if the acceleration of the ground motion exceeds a limit level. In 1996, UrEDAS (Urgent Earthquake Detection and Alarm System) has been developed. At the moment there are 19 UrEDAS stations covering about 1000 km along the Shinkansen line from Tokyo to Hakata. In the case of an earthquake, each station estimates the potential damage area within 3 seconds after detecting the P-wave, and issues an alarm to cut off the power supply for the Shinkansen trains if necessary. UrEDAS is a unique early warning system because it can determine seismic parameters with P-wave data from only one station (single station approach), and can issue the alarm based on the ground motion exceedance of a threshold defined on observed damages of previous earthquakes.

Espinosa-Aranda et al (1995) in 1991 developed an EWS for the protection of Mexico city. The system has been implemented after the $M=8.1$ Michoacan earthquake. The system provides alerts to residents and authorities in order to evacuate large segments of population in case of damaging earthquakes in the Guerrero seismic gap, located at 300 Km from the city. The system started in

1991 in experimental mode for schools' alert and stop the metropolitan subway system. Later in the 1993 became a public service. After several months the system triggered the $M=5.8$ and $M=6$ earthquakes originated from the Guerrero gap fault giving an alert of 60 seconds. Till now the system has triggered more than 1783 earthquakes of magnitude in the range of 2.5 and 7.3 (Note: events of magnitude greater than 5 are felt in Mexico City). The EWS sent 46 alerts for magnitude greater than 6 and 11 with magnitude less than 6. More recently in November 2003 the EWS for Oaxaca region started in experimental mode. The alert signals are sent to schools, residential constructions, radio and television companies, emergency and civil protection agencies. A study on Mexico City EWS performance (Iglesias et al., 2005) reveals a high failure rate of the system. Iglesias et al. (2005) suggest that the causes are related to an innacurate algorithm and limited areal coverage of the network. The possible actions may be threshold adjustment and 40 additional stations in three concentric rings around Mexico City, as suggested by the authors. The proposed scheme refers to an algorithm that relates to a relationship between the root-mean acceleration in the epicentral area and the expected maximum acceleration in a reference site in Mexico City. Based on the analysis of Michocoan earthquakes since 1985 to present, a warning threshold of 5 gal for the root-mean acceleration for unfiltered records in the near-source is suggested for performance improvement of Mexico City EWS.

An EWS for Taiwan has been implemeted as part of the strong-motion instrumentation program (Wu et al., 1998). The "Taiwan Rapid Earthquake Information Release System-TREIRS" has been developed by Central Weather Bureau in 1995. This system has been refined and updated as a basis for the successive development of Taiwan EWS. The system TREIRS is composed by 97 digital telemetered strong-motion stations that continuously trasmitt seismic data to the Taipei central station. At the central station the data are continuously processed, in case a magnitude of 3.5 or greater event is recognized alert signals are sent trough fax, e-mail, pager and short message. The EWS for Taiwan is based on a virtual sub-network approach (Wu and Teng, 2002). The first 12 triggered stations are contributing to information for location and magnitude estimates. The analysis is concentrated only on a small number of stations of the network in order to reduce the reporting time and the volume of data to transmitt resulting in a gain in the warning time available.

The EWS works based on a sub-network approach able to issue an early alert to urbanized areas located more than 70 Km away from the epicenter. A window of 10 sec of waveforms from the stations is analysed and processed for the estimate of magnitude and location of the event. An empirical correction is applied to the magnitude estimate considering that S waves may not have arrived within the time window considered. A warning time of tens of seconds is available for the alert of areas located at 100 Km away from the epicenter, although is not a public service considering

that doesn't exist yet an education program for population. Is under development a program for instrumentation update, replacing the 16-bit digital accelerographs to 24-bit. A tsunami warning system is also under development.

Allen and Kanamori (2003) developed ElarmS for early warning application in Southern California. The system may issue alert in case of damaging event with few to tens of seconds of warning time. The system within a second after the earthquake origin estimates predominant period and event location based on P-wave trigger times, predominant frequencies and amplitudes. By using 2 seconds and 4 seconds of recorded data, respectively for low- magnitude earthquakes and for larger magnitude events, a good magnitude estimate is obtained.

The magnitude is evaluated using the relation obtained from a regression analysis as a function of the predominant period. Based on the estimate of magnitude and location ground shaking map is released within a second from the earthquake origin. The shake map is updated as more data become available and its accuracy increases with time.

Is under development an extension of ElarmS to Northern California. For the earthquakes representing a threat for the city of San Francisco a warning around 20 seconds may be available by ElarmS.

More recently the Japan Meteorological Agency developed a prototype warning system that alerts universities and private organizations, in case of seismic event. A national research project on EWS started in 2003 as a joint collaboration between Japan Meteorological Agency and other national agencies. Within a few seconds from the first trigger based on the first seconds of observation considering a single-station approach, hypocenter and magnitude are defined (Hirouchi et al., 2004). JMA has developed the EWS called Now-Cast for practical experiments. The network used for Now-Cast is composed by 800 seismometers distributed all over Japan with a inter distance of 25 Km, Hi-Net.

The seismometers are bore-hole installed at 100 m or deeper to eliminate noise. The central processing stations are located at JMA Tokyo and Tsukuba Information Center of NIED. The time to transmit data is about 2 seconds. By Hirouchi method seismic parametrs are estimated. A new algorithm for more accurate estimates is under development that combines Hirouchi and JMA method. Through a dedicated line and wireless communication system the information is transmitted to users represented by co-investigators of the project. Receiving systems based on the early information calculate shaking intensity of JMA scale and arrival time of S wave. During the experimental period, February and March 2005, the system triggered 740 events of which 100 were felt. The magnitude estimates were affected by an error of the order of 1 magnitude units, while

hypocenters were in the 99% of the cases correctly estimated. Future directions are related to more accurate and earlier estimates.

Under development is an EWS for the Lions Gate Bridge that is the main artery that connects the city of Vancouver to the North Shore municipalities of North Vancouver and West Vancouver.

The earthquake alert system is a network of seismometers/transmitters/receivers distributed throughout British Columbia, Washington and Oregon. The stations are connected together and to several central information processing hubs via high-speed telecommunication networks. The earthquake alert stations measure the primary vertical ground movements and transmit the data at a continuous rate to the central processing hubs, which, if an earthquake is detected, pass the earthquake warning on to adjacent sensing units and beyond according to the intensity of the earthquake that is in progress. Since high-speed telecommunication systems can pass along the warning (data) much faster than the speed of earthquake seismic waves, a substantial warning (in range of tens of seconds to minutes) is possible evaluated on the basis of a scenario analysis).

The scenario analysis has estimated a maximum time of 90 seconds and a minimum of 34 seconds, sufficient to turn to red the traffic lights and avoid a big number of vehicles to board the bridge, from 300 to 35, depending on the alert time available.

Another interesting case is the EWS for the nuclear power-plant, Ignalina, Lithuania (Wieland, 2000)

Seismic EWS can contribute significantly to the reduction of the seismic risk in nuclear power plants. This is particularly true for areas of high seismicity.

An early warning system for power plants produces the following benefits:

- It reduces the risk of release of radioactive material during a strong earthquake.
- It reduces the consequential damage in heavy equipment (steam turbine generator, large circulation pumps, depressurization system of reactor pressure vessel, steam generator, etc.).
- It reduces the seismic risk and thus the amount of insurance coverage.
- An early warning system can be installed without interfering with power production
- It is a short-term solution for reducing the seismic risk; in the long-term, improvements of the critical components have to be implemented.
- Shutting the nuclear reaction or releasing control rods in various types of nuclear reactors requires only about three seconds of pre-warning time.

An EWS has been installed at the 2x1500 MW Ignalina Nuclear Power Plant (INPP) in Lithuania (Wieland, 2000). The reactor building was designed for peak ground accelerations related to the seismicity of the Baltic states but the structure, by a latter analysis, do not comply with the modern

standards of safety. Since shutting down the reactors was not possible, for economical and political reasons, an alternative solution has been studied. An EWS will provide to shut down the reactor before a hazardous earthquake might occur in the vicinity of INPP.

The system consists of six seismic stations encircling INPP at a distance of 30 km and a seventh station at INPP. Each station is made up by three seismic substations each 500 m apart, as in Fig.2.1, the ground motion is recorded and the data are transmitted to the control centre via telemetry.

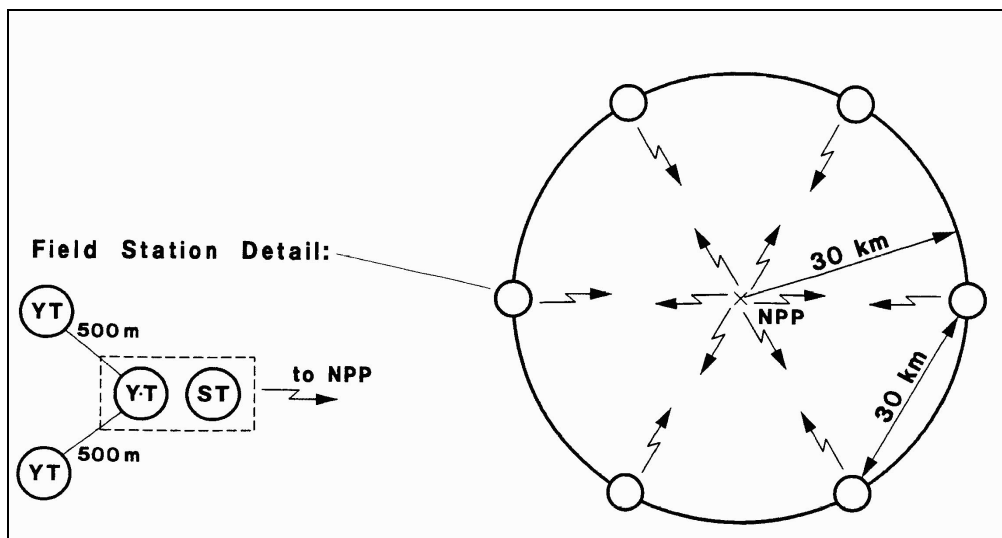


Figure 2.1 Earthquake early warning system for Ignalina Nuclear Power Plant (YT: accelerometer, ST:seismometer)

The seismic parameters are evaluated and on the basis of this information the appropriate action is taken. By continuous updates and by redundancy from several measurements at the same location, the problem of false alarms is reduced. For each seismic station, the cables are separated into three measurement channels up to the 2-out-of-3 voting logic located adjacent to the reactor control room, as in Fig. 2.2.

In the case the epicenter of the seismic event is included in the radius of 30 km, the time alarm is very short. To solve the problem, a seismic system is installed in INPP in order to release a seismic alarm. A time period of 2 seconds is required for the insertion of control rods (A rod, plate, or tube containing a material such as hafnium, boron, etc., used to control the power of a nuclear reactor. By absorbing neutrons, a control rod prevents the neutrons from causing further fissions) in the nuclear reactor, to prevent the meltdown in case of strong earthquake and to reduce substantially the nuclear thermal capacity. The existing seismic system has been improved to guarantee a warning time greater than 2 s.

The INPP Seismic Alarm System, described above, can provide 8.5 s of alarm, but considering the time required to transfer and to process the data, the time is reduced to 4 s.

The warning time available is sufficient for INPP EWS to release control rods in the reactor before the arrival of the seismic waves.

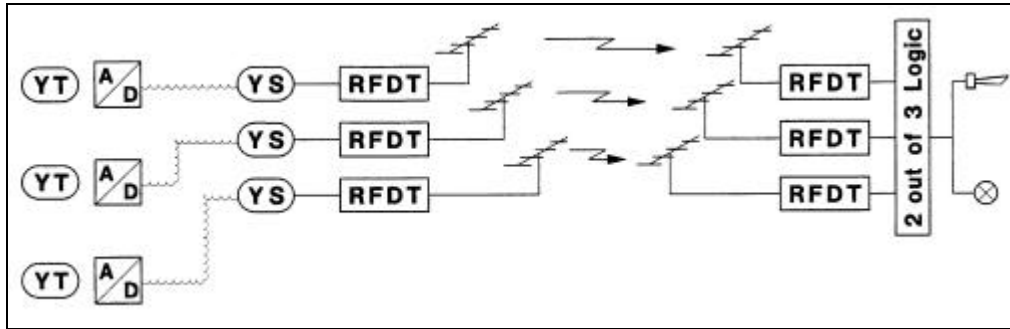


Figure 2.2 Seismic Alarm System (SAS): diagram of one of the six stations (YT: accelerometer, A/D: analog-digital converter, YS: seismic switch, RFDT: radio frequency data trasmission)

Wenzel et al. (1999) in the past years have developed an EWS for the protection of Bucharest, Romania. Hystorical data demonstrate that the earthquakes that represent a serious threat for Bucharest are intermediate depth Vrancea events (Oncescu et al 1999). The epicentral area is located at 130 Km from the city. This allows a warning time of half a minute for Vrancea events representing a similar case to Mexico City having a known epicentral area at a significant distance from the urbanized area. The estimated warning time is about 25-30 seconds.

Ground shaking prediction in Bucharest is done based on a scaling relationship between observed P-wave amplitude at the epicenter and S-wave amplitude at Bucharest. This consideration saves precious time, avoiding the need of an accurate estimate of magnitude and location for an accurate estimate of ground shaking at a site of interest.

Scaling relations have been found for PGA, spectral acceleration and expected intensities at Bucharest. The EWS for Bucharest is in operation officially since 2005.

Campania Region represents an interesting application for EWS. Moderate to high intensity earthquakes represent the threat for a high densely populated area as Campania. The most recent event is the 1980 M=6.9 event with epicenter localized in the Irpinia at 80-100 Km from the city of Naples. Recently a project on the development of an EWS for Campania Region has been funded by Regional Department of Civil Protection (Zollo et al. 2005). The warning time available for activation of security measures before the shaking initiates varies between 14-20 sec, at 40-60 Km of epicentral distance, and 26-30 seconds at 80-100 Km. This time of warning enables the possibility of activating several security measures for the protection of strategic infrastructures

(hospitals, bridges, schools, etc.) from a seismic threat. The EWS is based on a sub-network approach to reduce time consuming, decision and processing is in this way distributed to the nodes of the network, located in the source zone. Local control centers receive information from the nodes and communicate with the central unit, in Naples. Each single node based on the first seconds of P-waves is able to communicate to the closest local control center estimates of origin time, magnitude and location of the event. As more stations are triggered and as more data become available, the nodes refine their estimates. The local control center receives in real-time the estimates from the nodes and compares the information coming from the nodes for the sake of accuracy. The information will only then be sent to the central unit in Naples. Location estimates are done by the use of Voronoi cells, defining the most likely locations based on the triggered stations. Magnitude prediction models will be based on P-wave ground motions observed at near-source.

Virtual Seismologist (VS) (Cua and Heaton, 2004) method is a Bayesian framework based approach to early warning. Vs method uses prior knowledge as prior seismicity, Gutenberg-Richter law, Voronoi cells and real-time data from the stations during the seismic event. From acceleration, velocity and displacement observed in real-time the VS method estimates the most likely location and magnitude by maximizing the likelihood function. Based on the initial 3 seconds of P-waves coming from the first station magnitude is estimated from the ratio of the acceleration to the displacement. Location is based on Voronoi cells that define the most likely locations. In the first phase of the event prior information becomes essential for solving the trade-off between magnitude and location. As more stations are triggered and as more data become available the estimate become more accurate. Recently the method accuracy is being tested for bigger events as Chi-Chi earthquake (Yamada and Heaton, 2005).

2.3. Innovative EWS applications: Structural Control

Possible interaction between EWS and Structural Control is a quite recent subject still to be fully investigated. A general description of the potentialities of an EWS applied to the structural control of buildings has been first discussed in (Kanda et al. 1994; Occhiuzzi et al. 2004).

Performance of structural control systems can be improved by a preventive knowledge of the incoming seismic event. Relatively to passive Structural Control, according to the forecasting operations of the EWS, passive but property-adjustable devices could be fine-tuned in order to optimize the expected structural response based on the knowledge of the intensity and of the frequency content of the upcoming earthquake. The time needed to adjust the physical behavior of the devices would be about 10 s. In case of semi-active structural control system, according to the estimated properties of the upcoming earthquake, the most appropriate combination of control

algorithm and device properties could be selected and EWS could start the warm-up of the control system before the shaking initiates. As an example, consider a semi-active magnetorheological damper. By varying the intensity of the magnetic field inside the damper, it is possible to command to the device a fairly wide range of physical behaviours (Dyke et al.1996, Occhiuzzi et al. 2003, Yang et al. 2002). In this case, by an a priori knowledge of intensity and frequency content of the upcoming earthquake, it is possible both to set up the initial value of the magnetic field and to select the most appropriate operation logic, i.e. the control algorithm among those numerically investigated in a multi-scenarios analysis. The time needed to update the semi-active control system would be of about 1 s. Finally, in the case of active structural control systems, an early warning system could make possible to start the autonomous production of electric energy or to activate some different form of energy storage in order to make the control system work during the time interval corresponding to higher values of the ground motion. Furthermore, the adoption of feed-forward control loops, whose effectiveness in earthquake response reduction is largely unexplored (Mei et al. 2000), could be looked at from a different perspective if an estimate of the incoming disturbance were available.

2.4. Prediction Methods: examples

2.4.1. ElarmS

Based on the consideration that P-waves represent an important information carrier on the size of the incoming event, Elarms has been designed for seismic risk mitigation in Southern California, issuing an alarm ahead of time, before a damaging seismic event occurs (Allen and Kanamori, 2003).

The ElarmS methodology is designed to provide the most rapid assessment of the hazard posed by an earthquake as possible. A first hazard estimate is possible one second after the first P-wave trigger. By using the information contained within the P-wave a warning may be issued before significant ground shaking occurs at the surface, i.e. before the S-wave at the epicenter. The methodology is described by Allen and Kanamori (2003) and Allen (2004), here we briefly review the components of the ElarmS methodology that are important in the following error analysis.

Event location is determined from the P-wave arrival times. When the first station is triggered the epicenter is located at that station with a typical depth for the region. When the second station triggers the epicenter is located between the two stations, and then between the first three stations. When four stations have triggered the location is determined by a grid search to minimizing residual times. Magnitude is estimated using scaling relations between the predominant period of the P-wave within the first 4 seconds and event magnitude (Nakamura, 1988; Allen and Kanamori, 2003;

Lockman and Allen, in press; Olson and Allen, in press; Lockman and Allen, in review). For southern California two scaling relations have been defined (Allen and Kanamori, 2003). Initially, an event is assumed to be “low” magnitude ($3.0 < M < 5.0$) and the predominant period of the P-wave is determined from the vertical velocity waveform having low-passed the data (using a recursive real-time filter) at 10 Hz. The magnitude is then estimated from the maximum observed predominant period, T_{\max}^P , using the relation:

$$M = 6.3 \log(T_{\max}^P) + 7.1 \quad 2.3$$

If the magnitude estimate for a given event becomes greater than M 4.5, then T_{\max}^P is determined from a waveform that has been low-pass filtered at 3 Hz and the magnitude is estimated from the relation:

$$M = 7.0 \log(T_{\max}^P) + 5.9 \quad 2.4$$

The first magnitude estimate is available one second after the first station has triggered. As time progresses and more of the P-wave at the first station is available, the magnitude is updated if T_{\max}^P increases. As additional stations trigger the event magnitude is defined as the average of individual station estimates.

Given the event location and magnitude, the distribution of ground shaking is estimated using attenuation relations. Most published attenuation relations focus on large magnitude events (e.g. Newmark and Hall, 1982; Abrahamson and Silva, 1997; Boore *et al.*, 1997; Campbell, 1997; Sadigh *et al.*, 1997; Somerville *et al.*, 1997; Field, 2000; Boatwright *et al.*, 2003). ElarmS is intended to be operational for $M > 3$ earthquakes and therefore uses its own simplified attenuation relations. The attenuation model used for southern California is defined as:

$$\log_{10} PGA = 0.7179M + 2N - N \log_{10}(R) - 3.2373 \quad 2.5$$

where PGA is the peak ground acceleration, M is the magnitude, R is the epicentral distance and N is a coefficient which is a function of the magnitude (Allen, 2004).

2.4.2. VS method

The magnitude-estimation method, described in the virtual seismologist method (Cua and Heaton 2004), consists in predicting magnitude and epicentral distance and updating the informations as more real-time data become available. The prediction of magnitude and epicentral distance, “posterior”, is based on a bayesian approach, accounting for an a-priori knowledge of the phenomenon, “prior”, and for the observations of the upcoming event, “likelihood”. The “prior” represents the knowledge related to the expected values of magnitude and location, before analyzing the observations. The real-time data are used to define the “likelihood” that represents magnitude and location predictions based on the observations of the first seconds of P-waves; as the first station is triggered, the most probable values of magnitude and epicentral distance are defined from the observed ground motion amplitudes, considering the first seconds of real-time registrations. The most-likely magnitude and locations, related to the observed ground motion amplitudes, will be compared to a prediction of magnitude based on the following equation:

$$M = -1.627 \times Z_{ad} + 8.94 \quad 2.6$$

where:

$$Z_{ad} = 0.36 \log(PGA) - 0.93 \log(PGD) \quad 2.7$$

and PGA and PGD are, respectively, the observed peak acceleration and displacement for the considered station and Z_{ad} is defined as ground motion ratio. Assembling the most likely values of magnitude and location from the amplitudes observations and the most-likely magnitude as a function of the ground motion ratio, it will result a consistent “likelihood” prediction of magnitude and epicentral distance. As more stations are triggered and as more data become available, the prediction will be updated. The predicted values of magnitude and epicentral distance, considering one of the described methods, are then used to predict the ground motion amplitudes.

In the VS method (Cua and Heaton 2002) the amplitude is defined as:

$$\begin{aligned} \log(A) = & aM - b \times (R_1 + C(M)) + \\ & -d \log(R_1 + C(M)) + e + \varepsilon \end{aligned} \quad 2.8$$

where M is the magnitude; R_1 depends on R which is the epicentral distance; $C(M)$ is a correction factor depending on magnitude. The residual term ε is a zero mean error term representing the prediction uncertainty and e is a constant error which includes station corrections; the parameters a , b , d , e are defined by the model’s calibration by data fitting.

Chapter 3

3. Seismic EWS from user's perspective

EWS design philosophy concepts may be found in the theory of ergonomics that is the discipline which focuses on the interaction among humans and other elements of a system, in order to optimize the overall system performance focusing on user's requirements (Grasso et al. 2004 c). The design of an ergonomic system relies on user's requirements, represented by human needs (Genaidy et al. 1999). In the case of EWS design the end user is represented by the system to protect, that may be a structure, an infrastructure, a bridge, an urbanized area, transportation system, etc; Important lessons can be learned from ergonomics, as a fundamental guideline for the design philosophy of both the systems, EWS and control system for security measure activation in case of alarm.

Based on the concept of a whole single system composed by EWS and control system, the design process for system optimization should be planned backward, focusing on the objectives (represented by user design requirements, in terms of time required for security measure activation, type of predictor required for the control system, quality level of the predictor, and tolerable level of probability of wrong decisions), going to the EWS design; on the other hand, the control system should be designed based on the "early" information, that could be available from an EWS.

In order to work as a whole system, the design of the single components should rely on the requirements of other components. Based on these considerations, feasibility of the interaction of control system and EWS and global system's reliability can be achieved focusing on the definition of the most appropriate precursor information, threshold calibration and uncertainty propagation for the evaluation of the consequences of taking action.

The EWS design is based on the requirements:

1. Warning time required for the security measure activation
2. Type of predictor (required by the control system)
3. Quality of the predictor (Error Analysis)
4. Tolerable level of probability of making wrong decisions

In this sense the design process will be based on the analysis of the EWS application to realize, the evaluation of user requirements, definition of the most appropriate information (predictor) required ahead of time on which the decision (alarm activation or do nothing) will be based, uncertainty analysis to define the error associated to the predictor, reliability assessment based on the expected probabilities of making wrong decisions, evaluation of the tolerable levels of probability of wrong decisions and alarm threshold setting.

Each step of the process will be described in details in the following Chapters 4, 5, 6. Error analysis and type of predictors description will be addressed in Chapter 4. Assuming to have selected the most convenient predictor, seismic EWS requirements may be synthesized as timeliness and accuracy of predictions. The system has to guarantee a certain performance together with timeliness representing a fundamental aspect for user's response before the strong motion is activated at the site.

The conflicting requirements of timeliness and reliability are often an issue and, up-to-date, are not considered properly in the EWS design process.

From a review of existing EWS applications emerges a mandatory need of including user perspectives in the design of the system. This chapter will introduce basic concepts in order to take into account user requirements in terms of the consequences of taking action as a fundamental step in the feasibility assessment of an existing EWS application and in the system design process of new applications.

3.1. Time required for security measure activation

The main goal of an EWS for earthquakes is the reduction or prevention of loss of life and mitigation of structural damage and economic loss. The benefits of EWS are due to the measures that can be carried out from the moment in which a seismic event is detected at a certain place until the moment in which the seismic waves arrive at a location of interest. These measures, for prevention or emergency response, can be categorized by considering the phases of the seismic event (Wieland, 2001).

After event detection but before the earthquake arrives at a site, the warning provided by EWS with pre-arrival times of up to perhaps 90 seconds, could be used to evacuate buildings, shut-down critical systems (such as nuclear and chemical reactors), put vulnerable machines and industrial robots into a safe position, stop high-speed trains, activate structural control systems (Kanda et al. 1994, Occhiuzzi et al. 2004), and so on.

During an earthquake, the alarm generated by EWS could still enable such mitigation processes to be activated if there was insufficient time to do so prior to the arrival of the earthquake at the site. Within seconds after an earthquake, the information provided by EWS could be used to produce damage and loss maps based on the ground shaking intensity and could be the basis for more effective emergency response and rescue operations.

Evacuation of at-risk buildings and facilities is only feasible if the warning time is around 1 minute before the arrival of the strong shaking, which is possible only in the case where the seismic source zone is sufficiently far away. This is the situation, for example, for the threat to Mexico City from

earthquakes occurring in the subduction zone along the Pacific Coast (e.g. Lee and Espinosa-Aranda, 1998), where the time available is sufficient to alert large segments of the population by commercial radio and television, and for evacuation of strategic buildings, such as schools, crowded facilities, and so on.

In the case of a few seconds warning time before the shaking, it is still possible to slow down trains (e.g. Saita and Nakamura, 1998), to switch traffic lights to red (as for the Lions Gate bridge EWS, Vancouver), to close valves in gas and oil pipelines, to release control rods in nuclear power plants (e.g. Wieland *et al.*, 2000), activate structural control systems, and so on. In addition, secondary hazards can be mitigated that are triggered by earthquakes but which take more time to develop, such as landslides, tsunamis, fires, etc., by predicting the ground motion parameters for the incoming seismic waves. This could be used, for example, to initiate the evacuation of endangered areas.

Given that an appropriate EWS is in place for a local area or critical facility, its impact or effectiveness is dependent on the warning time available and the quality and reliability of the information that is provided, since these influence and constrain the utilization of the information. In most EWS applications, the available warning time is likely to be no more than tens of seconds, enabling the possibility of activating mitigation measures but meaning that automated activation is essential to fully utilize the available warning time.

3.2. Main aspects of consequences of prediction uncertainty

Suppose that the EWS works by setting an alarm if a critical shaking intensity threshold is predicted to be exceeded at a site, where the choice of critical threshold depends on the vulnerability of the system to be protected at the site, then based on the predictions from the first few seconds of P-waves observation, a decision has to be made of whether to activate the alarm or not. In making this decision, two kinds of errors may be committed (Wald, 1947) due to the uncertainty associated to the predictor on which the decision is based:

- Type I error: the alarm is not activated when it should have been.
- Type II error: the alarm is activated when it should not have been.

The type I errors are *missed alarms* and type II errors are *false alarms*; the probability of each of these wrong decisions can be therefore expressed as:

- P_{ma} = probability of missed alarm, that is the probability of having threshold exceedance but no alarm activation.
- P_{fa} = probability of false alarm, that is the probability of having no threshold exceedance but alarm activation.

The tolerance of a type I or II error is related to a trade-off between the benefits of a correct decision and the costs of a wrong decision and it could vary substantially, depending on the relative consequences of possible missed and false alarms. For example the automated opening of a fire station door has minimal impact if the door is opened for a false alarm. On the contrary, an automated shutdown of a power plant could cause problems over an entire city and involve expensive procedures to restore to full-operational status. In this latter case, the EWS must be designed to keep the frequency of false alarms very low.

In general, the automated decision process has to be designed with attention focused on the probability of false and missed alarms along with a cost-benefit analysis. Some mitigation measures could be unacceptable to operate as a result of the false or missed alarm rate being too high.

The probability of a wrong decision is due to having only partial knowledge of the phenomenon and so any prediction, as a consequence, is affected by uncertainty. A key element of an EWS is a better understanding of the parameters that play a fundamental role in the uncertainty, and hence the quality of the predictions on which decision making is based. Reliability and feasibility of EWS, will be analysed both for new applications and for feasibility assessment of existing EWS applications.

3.3. Definitions

Lets clarify the terms that will often be used in the following chapters, representing important aspects of EWS (Grasso et al., 2005 a,b).

- Critical Threshold (a): defined by a parameter a that represents the value of the predictor related to the occurrence of heavy damage and/or economic losses. The critical threshold is a known parameter of the design process. For structural applications of EWS the critical threshold may be represented by occurrence of structural damage or collapse, depending on the damage level of interest, the value of the threshold is defined by vulnerability assessment. For industrial applications the critical threshold may be defined by risk analysis.
- Warning (Alarm) Threshold ($c \cdot a$): The alarm threshold corresponds to the value of the predictor for which activate the alarm. To control the probability of wrong decisions, the warning threshold is chosen as the product of the critical threshold a and a parameter, c , to be specified during the design process. The warning threshold $c \cdot a$ depends on the design process chosen to optimize the automated alarm activation system. The design parameter c provides a mechanism to control the incidence of false and missed alarms. The coefficient c is a parameter that will be defined in the design process, based on consequence based

approach. Two approaches are possible: time-invariant approach providing fixed alarm threshold (Fig. 3.1 and 3.2) and time-variant approach for the definition of a time-varying alarm threshold (Fig. 3.3 and 3.4). These concepts will be explained in detail in the following Chapters 6-7. The coefficient c will be greater than unit if we are more concerned about false alarms and less than unit if we are more concerned about missed alarms.

- Tolerable level of probability of wrong decision: based on a cost-benefit analysis is the level of probability of false alarm (β) or missed alarm (α) that can be accepted based on the consequences of false and missed alarm, expressed in monetary costs or loss of lives etc. For example a nuclear power-plant is characterized by a high cost of false alarm due to the expensive procedures to restore the full operational status of the plant, on the contrary for population alert, as for Mexico City EWS, the cost of a missed alarm is much higher compared to the cost of a false alert.
- P_{ma} = probability of missed alarm, that is probability of having critical threshold exceedance but no alarm activation,
- P_{fa} = probability of false alarm, that is, probability of having no critical threshold exceedance but alarm activation.

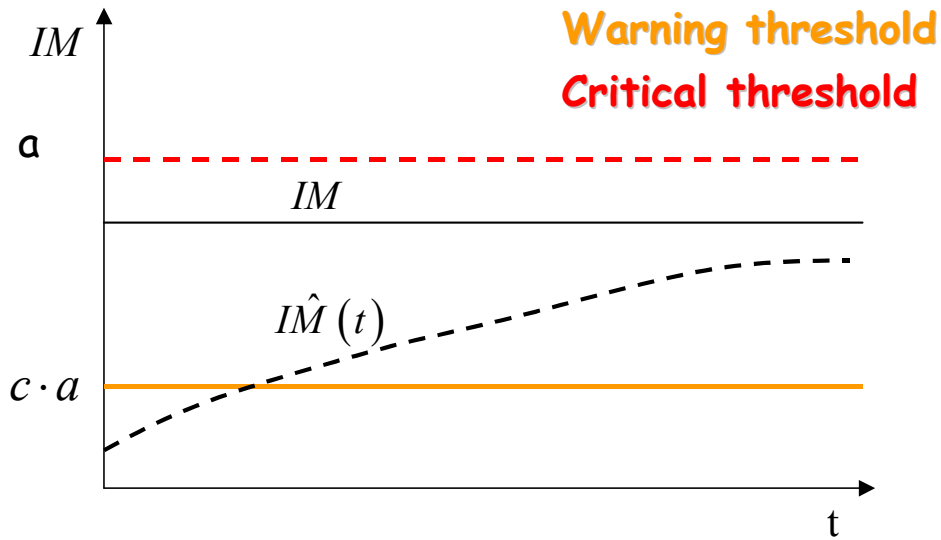


Figure 3.1 False alarm in the time-invariant approach. In the figure is represented IM that is the actual value of the predictor, \hat{IM} is the predicted value as a function of time, in the red dashed line is represented the critical threshold and with the orange line the warning threshold. Note the warning threshold is time independent. False alarm is represented by the situation of alarm activation (warning threshold exceedance of the predictor) when we should have not (no critical threshold exceedance of the actual value).

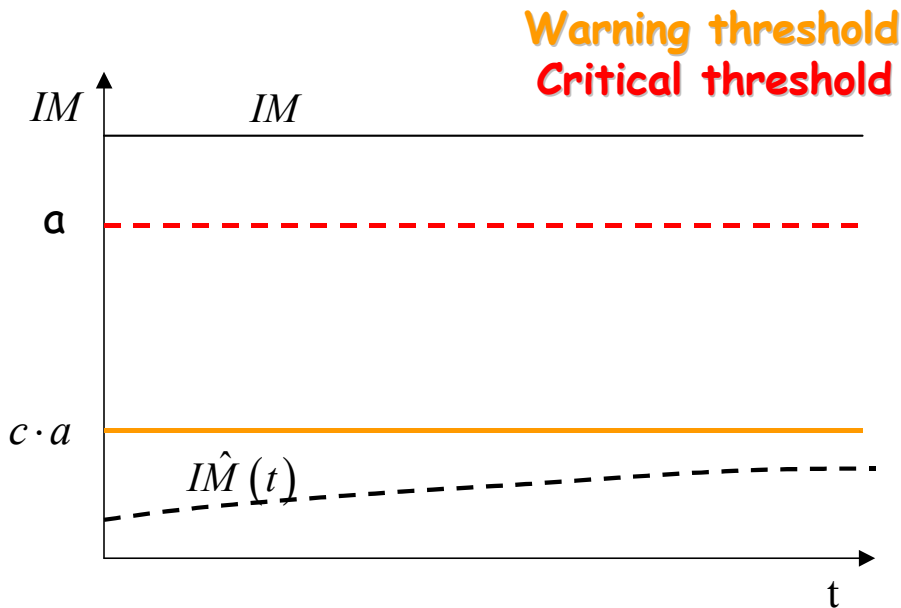


Figure 3.2 Missed alarm in the time-invariant approach. In the figure is represented IM that is the actual value of the predictor, \hat{IM} is the predicted value as a function of time, in the red dashed line is represented the critical threshold and with the orange line the warning threshold. Note the warning threshold is time independent. Missed alarm is represented by the situation of no alarm activation (no warning threshold exceedance of the predictor) when we should have (critical threshold exceedance of the actual value).

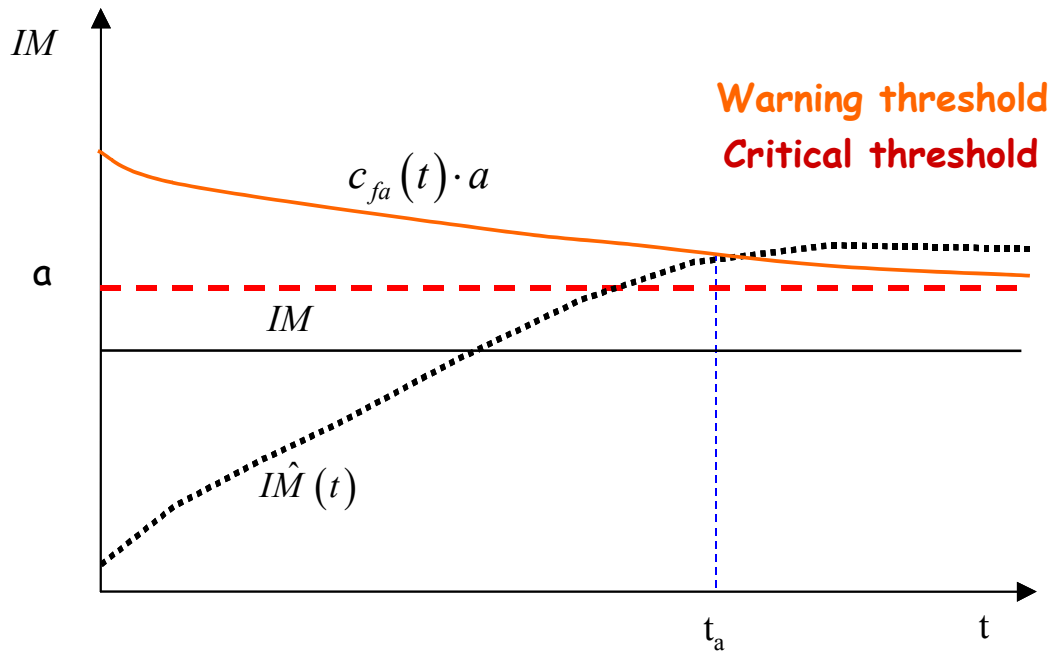


Figure 3.3 False alarm in the time-variant approach. In the figure is represented IM that is the actual value of the predictor, \hat{IM} is the predicted value as a function of time, in the red dashed line is represented the critical threshold and with the orange line the warning threshold. Note the warning threshold is time dependent. False alarm is represented by the situation of alarm activation (warning threshold exceedance of the predictor) when we should have not (no critical threshold exceedance of the actual value).

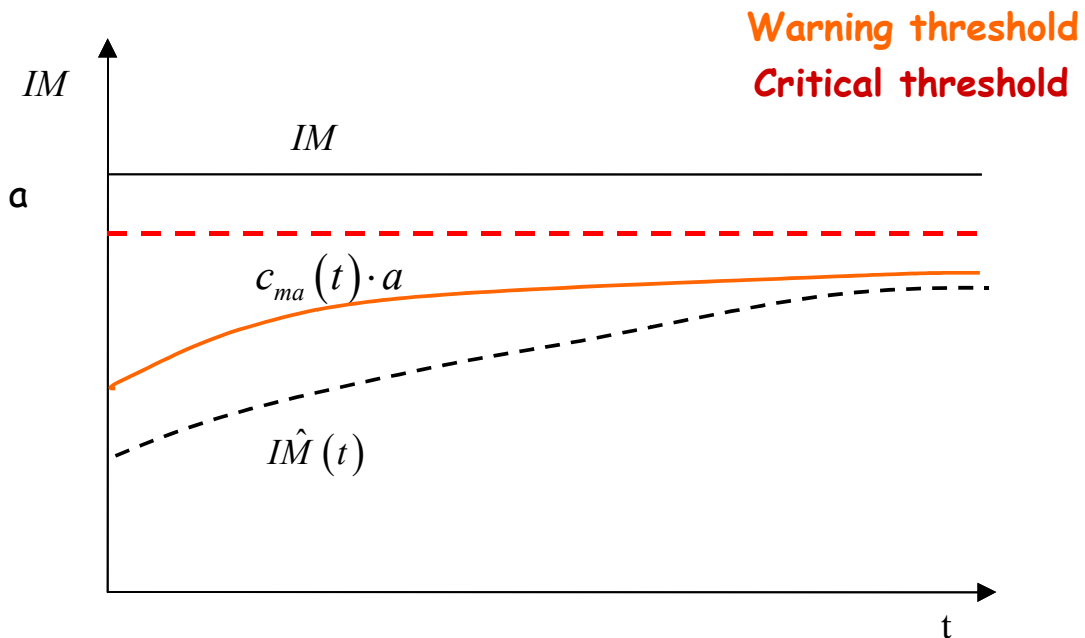


Figure 3.4 Missed alarm in the time-variant approach. In the figure is represented IM that is the actual value of the predictor, \hat{IM} is the predicted value as a function of time, in the red dashed line is represented the critical threshold and with the orange line the warning threshold. Note the warning threshold is time dependent. Missed alarm is represented by the situation of no alarm activation (no warning threshold exceedance of the predictor) when we should have (critical threshold exceedance of the actual value).

Chapter 4

4. Uncertainty Analysis

A fundamental aspect of an EWS, for feasibility assessment or real-time decision making, is represented by a better understanding of the quality of the predictions on which decision making is based. A first review of EWS prediction process will help to underline the parameters that play a fundamental role in prediction uncertainty. A description of the probability models of the errors associated with each of these parameters follows. Finally prediction uncertainty is obtained by uncertainty propagation, two methodologies are proposed. The ElarmS methodology (Allen and Kanamori, 2003) is analysed as a case study in order to determine the total uncertainty associated with the ground shaking prediction at a site of interest.

4.1. EWS prediction process and predictors

The prediction model for the ground motion parameters can be represented as a sequential multi-compartment model, composed of two sub-models, M_1 and M_2 (Grasso et al., 2005 c), in which outputs of M_1 are inputs to M_2 but inputs and outputs of M_2 cannot be inputs to M_1 .

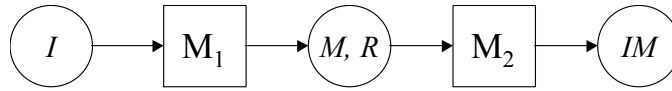


Figure 4.1 The multi-component model representing EWS, Bates et al. (2003). M_1 is the earthquake predictive model; M_2 is the attenuation model; I is the synthetic information extrapolated from the data from the stations; M is the magnitude; R is the epicentral distance; IM is the intensity measure representing the shaking intensity.

M_1 is the earthquake predictive model, which estimates earthquake parameters (magnitude, M ; epicentral distance, R), based on parameters, I , from real-time measurements of the first seconds of P-waves, e.g., I is the predominant period in Allen and Kanamori (2003); I is the observed ground motion ratio for the Virtual Seismologist method in Cua and Heaton (2004).

The ground motion attenuation model, M_2 , predicts a ground motion parameter (IM), based on the magnitude and epicentral distance predicted by M_1 . The parameter IM , which could be the final outcome of the EWS prediction process, represents the predicted ground motion intensity (PGA, PGV, S_a , etc) that will occur at the site where a strategic facility of interest is located and it is the predictor on which the decision to take some protective action is based. The decision may be based on other parameters of interest (i.e. engineering demand parameters, expected losses, etc.), in this case the IM represents an input parameter of another prediction model (M_3). A modified model that can be used for the estimate of other predictors may be represented as a multi-compartment model.

The EWS model described previously is a two-compartment model (M_1 and M_2) whereas a single compartment model (M_3) able to predict the relevant parameter can be adopted (Grasso et al. 2004 c).

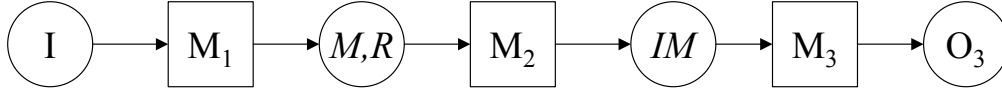


Figure 4.2 The multi-component model representing EWS for engineering demand parameter prediction, Grasso et al. (2004). M_1 is the earthquake predictive model; M_2 is the attenuation model; I is the synthetic information estrapolated from the data from the stations; M_2 is the predictive model of engineering demand parameters; M is the magnitude; R is the epicentral distance; IM is the intensity measure representing the shaking intensity; O_3 represents the predicted engineering demand parameter.

For example for structural applications the decision might be based on engineering demand parameters. It is important to point out that the predictor intensity measure provided by an EWS, expressed in terms of ground motion amplitude (usually PGA , PGV), cannot represent a convenient tool for the prediction of the dynamic behaviour of the structure, that perform in a non-linear and multi-degree-of-freedom behaviour. For a better prediction of the structural behaviour, in order to optimize the decision making for the activation/design of the control systems a few seconds before the occurrence of the ground motion, a more representative parameter should be taken in account. For example, response parameters correlated with drift demand δ are generally agreed to significantly represent the structural behaviour. A relationship between the drift and the intensity measure (represented by the model M_3) could therefore represent an effective tool for the prediction of the structural behaviour. The structural behaviour should be foreseen on the basis of the predicted intensity measure, which is the output of the ground motion prediction process of an EWS. Barroso and Winterstein (2002) have proposed the relation between ground motion intensity measure, expressed in terms of spectral acceleration, S_a , and the structural parameter, $\hat{\delta}$, representing the median drift demand:

$$\hat{\delta} = aS_a^b \quad 4.1$$

where the coefficients a and b are obtained by fitting observed data, obtained by non-linear incremental dynamic analysis, (Vamvakistos and Cornell 2000). In this case, Barroso and Winterstein have considered a steel moment-resisting frame excited by synthetic ground motions obtained for different values of S_a . The drift demand is related to the median drift demand by:

$$\delta = \hat{\delta}(S_a) \cdot \varepsilon \quad 4.2$$

The parameter ε defines the variability of the values of δ compared to the median value.

For structural control application the predictor may be the expected behaviour of the controlled structure, that is expressed as (Barroso and Winterstein 2002):

$$\hat{\delta}_c = a_c S_a^{b_c} \quad 4.3$$

where the index c is addressed to the controlled structure and the coefficients a_c and b_c are obtained from structural analyses on different structures in controlled configuration.

Other predictor to take in account in the decision process may be probability of false and missed alarm, structural damage, economic or loss of lives, that represent the consequences of the action of activating the alarm or not (see Chapter 8).

4.2. *Uncertainty Analysis*

Uncertainty analysis represents an important tool for feasibility assessment of EWS application, based on the uncertainty of the prediction.

The estimate of the uncertainty associated with the prediction is a fundamental information in order to evaluate the expected consequences of a decision in real-time analysis. A method for uncertainty analysis is described in the following sections. Is presented a frame-work for evaluating the error associated with the prediction, useful for comparing the performance of existing prediction models of real-time seismic parameters, isolating the single errors source of uncertainty in order to define the mitigation strategies to reduce the total error.

A single station approach for ground motion parameter prediction is described and the error associated with the estimate is evaluated, underlining the possibility of defining the effects and the advantages of waiting for additional information.

The attention is focused on the uncertainty of the predictor on which the decision of raising the alarm or not is based.

In this report, the predictor (quantity of interest) is taken to be a ground motion parameter that represents the shaking intensity at the site of the facility. The prediction is based on a partial knowledge of the event (first second of P-waves) and represent the output of predictive models, associated to an error as well. The total uncertainty associated to the predictor will be decomposed in single uncertainties, sources of uncertainty; each error will be analysed and modeled by the means of probability distribution function and the total uncertainty will be defined.

4.2.1. Sources of uncertainty

Uncertainty in the predictor IM is a result of the uncertainties in the models M_1 and M_2 , including the prediction errors related to the magnitude, the source location, and the attenuation model.

The source of the uncertainties for each model is represented in the following figure, where ε_M , ε_R and ε_{IM} denote the uncertainties related to the magnitude and location prediction model and to the attenuation model, respectively.

Uncertainties of each sub-model propagate through the output, so each uncertainty plays an important role in the definition of the final quality of the intensity measure, IM .

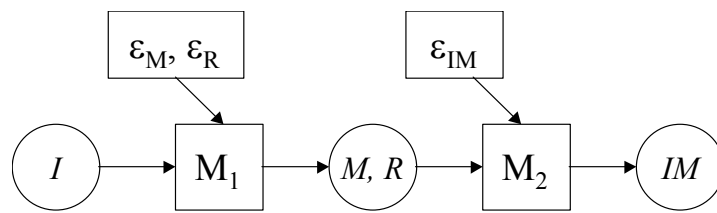


Figure 4.3 The multi-component model for EWS uncertainty propagation. M_1 is the earthquake prediction model and M_2 is the ground motion attenuation model

A Gaussian distribution model is chosen for ε_M and ε_{IM} to model the magnitude and attenuation model uncertainties. The uncertainty of the predicted magnitude can be well modeled as a Gaussian distribution, as confirmed by Grasso and Allen (2005) and Cua and Heaton (2004), with a standard deviation dependent on the prediction model (e.g., the magnitude error has zero-mean and a standard deviation of 0.4 for the Heaton-Cua relation and it decreases with increasing number of data). According to the Allen-Kanamori method, the uncertainty of magnitude prediction, is related to the number of stations considered and to the elapsed time, and it assumes a value of 0.7 (in magnitude units) considering only one station, 0.6 for three stations, 0.45 for five stations, and it drops to 0.35 if ten stations are considered (Allen, 2004).

Errors related to ground motion amplitude are modeled well by a lognormal distribution, i.e. if the intensity measure IM is the natural logarithm of the ground motion parameter, then IM can be assumed to be Gaussian. This hypothesis is confirmed by the analysis done by Grasso and Allen (2005) for the analysis of ElarmS uncertainty and by Cua and Heaton (2004) in which the errors, evaluated based on a large number of data and considering ground motions recorded by the seismic network in Southern California over 4 years, were analysed.

Related to the uncertainty in epicentral distance prediction, in the case of large magnitude teleseismic events, the probability of a large prediction error based on the first few seconds of data

is likely. In fact, in this case the network could erroneously locate the epicenter inside the instrumented area (Kanamori and Heaton 2004, personal communication). To avoid epicenter mislocation, in case of teleseismic events, is important to exclude the case in which the triggered stations are the perimetral ones and for which the amplitude of P waves is small, as confirmed by Kanamori (2004)

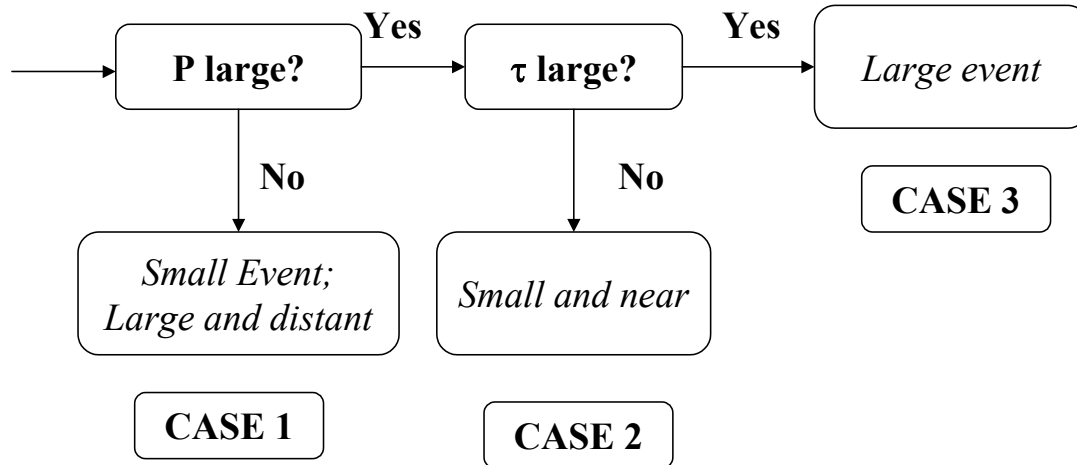


Figure 4.4 The P wave amplitude is a key parameter in identifying immediatly the level of intensity of the incoming event, P waves are an important information carrier. If the P wave amplitude is small we are in the case of small or teleseismic event, if the P wave amplitude is large we have to look at the predominant period, τ . If τ is small the event is small and near, if is lare the event is a large event. (Kanamori, 2004).

For epicenter mislocation is important to exclude the stations triggered by events that are not seismic (noise) (Allen personal communication). Excluding these cases the epicentral distance error can be modeled as a lognormal distribution, or equivalently as a Gaussian distribution considering the variable $\log R$, instead of R .

4.3. Uncertainty propagation

Our trust in EWS depends on the expected levels of error committed in the prediction. It is necessary to estimate the error in order to quantify the performance of the EWS prediction process.

Two different methods will be described for uncertainty propagation:

1. uncertainty propagation method
2. numerical Monte Carlo method.

Uncertainty propagation method refers to an aproximation method based on first-order Taylor series expansion in order to evaluate the total error as a composition of the single errors, assuming independency of errors.

In the cases in which the aproximation method is not applicable the Monte Carlo method is suggested, that is a simulation method for uncertainty propagation of the single errors through the output. The two methods are fully decribed and an application of Monte Carlo method is analysed

for the evaluation of ElarmS (Allen and Kanamori 2003) performance (Grasso and Allen, 2005).

4.4. *Aproximation method for uncertainty propagation*

The aproximation method for uncertainty propagation is a method based on a first-order Taylor series expansion in order to quntify the total error associated with the predition. The predictor that will be considered is the intensity measure. The predictor is a function of magnitude and epicentral distance (in log scale) that in the uncertainty propagation process will be affected by errors, as shown in Fig. 4.3, and which are modeled and described by Gaussian distribution.

The prediction error is given by comparing the predicted intensity measure, \hat{IM} , to the actual IM :

$$\varepsilon_{tot} = \hat{IM} - IM \quad 4.4$$

where:

\hat{IM} is a function of the predicted values M , R and the uncertainties ε_M , ε_R and ε_{IM} :

$$\hat{IM} = f(\hat{M}, \hat{R}) + \varepsilon_{IM} = f(M + \varepsilon_M, R + \varepsilon_R) + \varepsilon_{IM} \quad 4.5$$

where the function f represents of the attenuation model, that in a general expression:

$$f(M, R) = \alpha + \beta M + \gamma \log_e R \quad 4.6$$

\hat{IM} represents the predicted value of intensity measure, dependent on M , R and the uncertanties ε_M , ε_R and ε_{IM} , that has to be compared to the actual intensity measure, IM , that is represented by:

$$IM = f(M, R) \quad 4.7$$

IM is a function of magnitude and location, M and R , where f is the ground motion attenuation model.

Under previous assumptions about ε_M , ε_R and ε_{IM} , the total prediction error follows a Gaussian distribution with mean and standard deviation that is depends on the means and standard deviations of these contributing prediction errors. As the quality of the prediction increases with increasing data, the standard deviation decreases and the uncertainty decreases.

The prediction error can be expressed as:

$$\varepsilon_{tot} = \hat{IM} - IM = f(M + \varepsilon_M, \log_e R + \varepsilon_{\log R}) + \varepsilon_{IM} - f(M, \log_e R) \quad 4.8$$

Based on the assumption of using M and $\log_e R$ as the basic Gaussian variables, the function may be expressed as a first-order Taylor series:

$$\begin{aligned}\varepsilon_{tot} &= \varepsilon_M \frac{\partial f}{\partial M} \big|_{(M, \log R)} + \varepsilon_{\log R} \frac{\partial f}{\partial \log R} \big|_{(M, \log R)} + \varepsilon_{IM} \\ &\approx \beta \varepsilon_M + \gamma \varepsilon_{\log R} + \varepsilon_{IM}\end{aligned}\quad 4.9$$

For given M and R the standard deviation is given by adding Gaussian variables which gives the variance of the sum equal to the sum of the individual variances under the assumption of independence of errors:

$$\sigma_{tot} = \sqrt{\beta^2 \sigma_M^2 + \gamma^2 \sigma_{\log R}^2 + \sigma_{IM}^2} \quad 4.10$$

where σ_{tot} is a function of time in relation with σ_M and $\sigma_{\log R}$ that are time dependent. As time progresses the standard deviation are updated and the total error σ_{tot} is evaluated. Eq. 4.10 allows a simple evaluation of the total error associated to the EWS prediction as a function of time. The mean of the total error is given by:

$$\mu_{tot} = \beta \mu_{\varepsilon_M} + \gamma \mu_{\varepsilon_{\log R}} + \mu_{\varepsilon_{IM}} \quad 4.11$$

in most of the cases may be assumed a zero-mean value for the total error distribution (Cua and Heaton 2004). If the empirically-derived models M_1 and M_2 (Fig. 4.3) are unbiased, then the mean $\mu_{tot} = 0$. In fact, μ_{tot} does have a value close to zero in the Virtual Seismologist method (Cua and Heaton 2004). If more complex attenuation models, or more complex probability models for ε_M , $\varepsilon_{\log R}$ and ε_{IM} , are used, this analytical approach may be not applicable and then a Monte Carlo method is suggested to quantify the uncertainty in ε_{tot} (Grasso et al. 2005 a,b).

4.5. Monte Carlo method for Uncertainty Analysis

Monte Carlo method for uncertainty propagation follows the same steps described for identifying the sources of uncertainty, defining the probabilistic models that describe the single errors and finally evaluating the total uncertainty associated with the predictor.

While with the uncertainty propagation method the total error is defined by using a first-order Taylor series expansion Eq. 4.9 considering $\log R$ as basic variable, with the Monte Carlo method the total uncertainty is defined by a Monte Carlo simulation to propagate uncertainties through the

system. The method is described with an application to ElarmS.

4.6. Monte Carlo method: quantifying ElarmS prediction error

We use a dataset of 32 earthquakes from southern California to estimate the errors in ground shaking predictions (Grasso and Allen, 2005). In order to assess the uncertainty if ElarmS was implemented in southern California, the event dataset consists of earthquakes recorded by the current dense seismic network close to the metropolitan areas, Fig. 4.5.

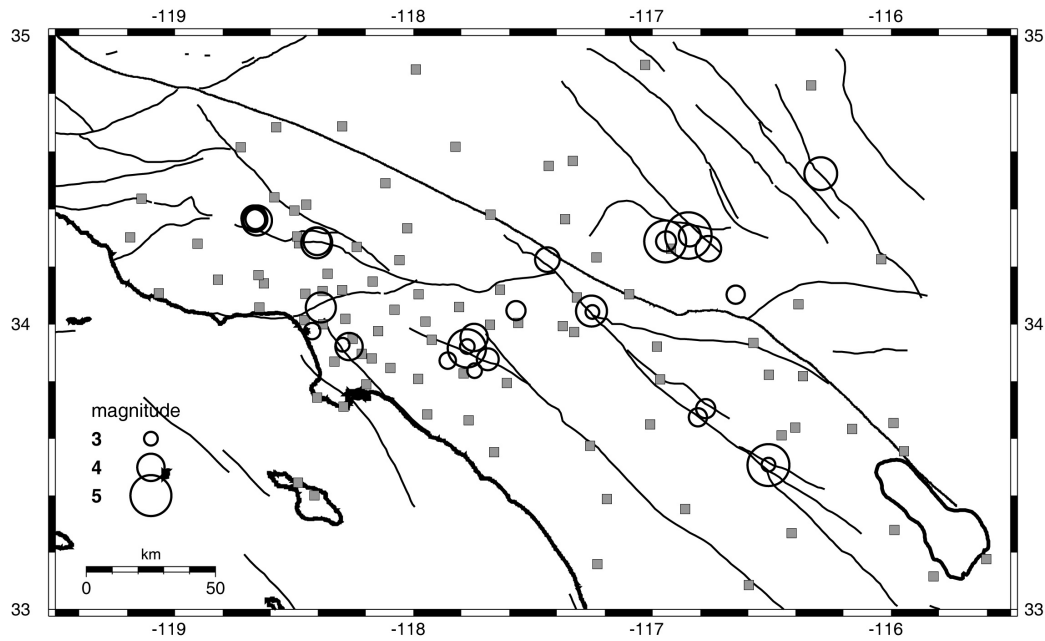


Figure 4.5 Map of the stations and earthquakes used in this study.

All the events occurred from 2000 to 2003 and have a local magnitude ranging from 3.0 to 5.4 (Table 4.1). The dataset does not include larger magnitude earthquakes as none have occurred beneath a dense seismic network as exists today. The waveforms were recorded by the California Integrated Seismic Network (<http://www.cisn.org>) and were obtained from the Southern California Earthquake Data Center (<http://www.data.scec.org>).

The ElarmS methodology can be represented as a multi-component model consisting of earthquake location, magnitude estimation and ground shaking prediction. The total uncertainty in a ground motion prediction can be derived from the individual errors in location, magnitude estimates using the predominant period, and the attenuation relations.

Date	Time	Magnitude	Latitude	Longitude	Depth	Number of stations	SCEDC event ID
02/21/00	13:49:43.10	4.3	34.047	-117.255	15.0	40	9140050
03/11/00	21:46:07.80	3.1	33.839	-117.744	3.5	7	9142593
09/16/00	13:24:41.30	3.2	33.976	-118.424	12.2	29	9163314
01/14/01	02:26:14.00	4.3	34.284	-118.404	8.8	55	9613229
01/14/01	02:50:53.00	4.0	34.289	-118.403	8.4	49	9613261
02/10/01	21:05:05.70	5.1	34.289	-116.946	9.1	58	9627721
02/13/01	03:04:35.60	3.5	34.289	-116.942	6.2	42	9628901
02/18/01	06:09:32.10	3.3	33.675	-116.809	16.7	47	9630113
03/25/01	00:41:25.20	3.4	34.048	-117.570	7.5	54	9639729
04/13/01	11:50:12.40	3.6	33.878	-117.688	3.6	59	9644101
04/20/01	09:52:12.20	3.4	33.705	-116.776	16.9	37	9645945
05/14/01	17:13:30.20	3.8	34.226	-117.440	8.7	63	9652545
07/03/01	11:40:48.10	3.9	34.264	-116.764	3.3	47	9666905
08/20/01	07:34:23.10	3.0	34.044	-117.250	15.7	45	9696461
09/09/01	23:59:18.00	4.2	34.059	-118.388	7.9	58	9703873
09/17/01	01:14:49.00	3.1	33.922	-117.774	11.8	40	9706897
09/23/01	22:44:32.00	3.0	33.509	-116.513	15.1	19	9708393
10/28/01	16:27:45.50	4.0	33.922	-118.270	21.1	60	9716853
10/28/01	16:29:54.60	3.0	33.929	-118.296	23.6	41	9716861
10/31/01	07:56:16.60	5.1	33.508	-116.514	15.2	45	9718013
01/29/02	05:53:28.90	4.2	34.361	-118.657	14.2	52	9753485
01/29/02	06:00:39.80	3.9	34.370	-118.668	14.2	52	9753489
01/29/02	06:08:01.80	3.8	34.365	-118.664	14.4	49	9753497
01/29/02	20:23:07.00	3.6	34.363	-118.667	12.6	45	9753949
01/30/02	18:47:57.30	3.5	34.366	-118.661	12.8	40	9755013
03/17/02	05:50:43.10	3.2	33.873	-117.856	9.5	38	12663484
04/05/02	08:02:56.00	4.4	34.524	-116.295	5.6	31	9775765
07/01/02	22:03:59.60	3.3	34.103	-116.651	10.0	33	9796589
09/03/02	07:08:51	4.8	33.917	-117.776	12.9	68	9818433
12/14/01	12:01:35	4.0	33.955	-117.746	13.8	70	9735129
02/22/03	12:19:10	5.4	34.310	-116.848	1.2	67	13935988
03/15/03	10:01:47	3.6	34.310	-116.843	3.8	41	13947424

Table 4.0 Earthquakes used in the analysis.

4.6.1. ElarmS Magnitude uncertainty

Error in ElarmS magnitude estimate has been evaluated as a function of time for the 32 events.

The error is defined as the difference between the prediction (Eq. 2.6 and 2.7) and the true magnitude determined by the network.

The time of the first trigger for each event is set to the zero time. In making this choice we assume that the amount of information about an earthquake, i.e. the number of stations recording P-wave information, increases in a similar fashion with time for all earthquakes. This assumption is reasonable for events occurring beneath the dense portion of the seismic network where the station spacing is approximately constant.

At 15 seconds from the first trigger, the error stabilizes and additional data will produce negligible effects in terms of error reduction. The magnitude error can be modeled as Gaussian distribution

with mean and standard deviation that varies as a function of time.

For each 1 sec of increment an error model is defined by fitting a Gaussian distribution to the errors to determine mean and standard deviation.

The error, when the first station is triggered, can be modeled as Gaussian distribution with mean equal to -0.45 and standard deviation of 0.61 , these values decrease to -0.25 and 0.41 , for mean and standard deviation, respectively, at 5 seconds from the first trigger, at 10 seconds the mean and the standard deviation assume the values of -0.14 and 0.34 , respectively, at 25 seconds the value of the mean goes to zero and the standard deviation assumes 0.26 .

t	μ	σ
1 s	-0.45	0.61
2 s	-0.3	0.47
3 s	-0.28	0.47
4 s	-0.28	0.46
5 s	-0.25	0.41
6 s	-0.2	0.39
7 s	-0.19	0.39
8 s	-0.18	0.37
9 s	-0.16	0.37
10 s	-0.14	0.34
11 s	-0.096	0.3
12 s	-0.08	0.26
13 s	-0.067	0.26
14 s	-0.06	0.26
15 s	-0.05	0.26
20 s	-0.045	0.26
25 s	-0.045	0.26

Table 4.1 Magnitude error is characterized by mean, μ , and the standard deviation, σ , function of time.

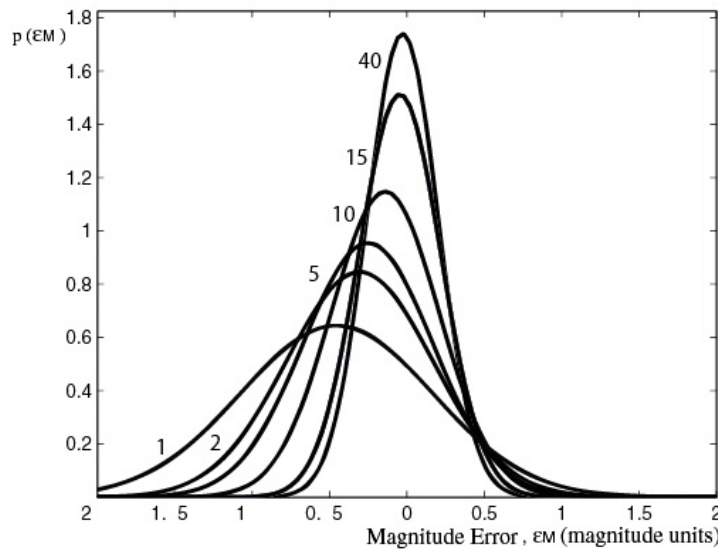


Figure 4.6 Magnitude error distribution as a function of time, considering the zero time the instant when the first station is triggered.

In the above analysis it has been assumed that the errors in \hat{M} from individual station observations, and in $P\hat{G}A$ at specific sites are the same. Improvements in the uncertainty of $P\hat{G}A$ can be made by taking both the individual stations and site errors into account. This is particularly important during the first few seconds of an earthquake sequence when data for a magnitude estimate is only available from a few stations. A recent study by Lockman and Allen (in press) determined the variability in the uncertainty in magnitude estimates from 22 stations in southern California. The average absolute magnitude error for the 22 stations varied from 0.13 to 1.02 magnitude units (see Lockman and Allen (in press) Figure 2), the corresponding range in the standard deviation was 0.18 to 1.57 magnitude units. A magnitude estimate based on observations from the best three stations in the Lockman and Allen study would have a standard deviation of 0.15 compared 0.41 when we treat the errors from all stations as being the same. In the case when it is the worst three stations the standard deviation would be 0.83.

The use of station-specific errors is perhaps most important in the real-time decision making process. Consider a scenario in which a specific user of the warning information receives a message predicting ground shaking above the threshold at which they would take action. When they first receive this warning the uncertainty may be large. However, if they know that 2 sec later, additional data is likely to reduce the uncertainty significantly, they may decide to wait for that information before taking action. Alternatively, if the uncertainty is unlikely to change, they will either initiate mitigating action immediately or not at all.

Different scenarios have been simulated, in which different combinations of stations have been chosen to be triggered. The error associated with the triggered stations in a single station approach

has been defined and then compared to the error models defined previously based on all the data available.

In the first scenario, three stations characterized by a little scatter of the period-magnitude relationship are considered, the magnitude error associated is defined by propagating the single-station errors.

The error is characterized by an uncertainty of 0.15 for the standard deviation, much less if compared to the 0.41 for the magnitude error for all the data.

In the second scenario the magnitude error has a standard deviation of 0.83, for 3 triggered stations characterized by a big scatter.

Finally the last scenario has been analysed in order to define the worth of waiting for more data, in the case the next station to be triggered is characterized by a high accuracy in the magnitude prediction.

In this scenario, if the first two stations to detect P-wave arrivals are those with the largest errors in Lockman and Allen's study (in press), the magnitude uncertainty would be 1.09. Based on the event location, the small subset of stations which will trigger next will be known along with their associated errors. If the third station to trigger is also a poor station the error will reduce to 0.83, but if it is a good station it will be reduced to 0.7 (Grasso and Allen, 2005).

Note that in the analysis the error associated with the averaged magnitude prediction has been evaluated based on the following equation:

$$\begin{aligned}\sigma_M &= \sqrt{\frac{(\sigma_1^2 + \sigma_2^2 + \dots + \sigma_n^2)}{n^2}} \\ &= \frac{\sqrt{(\sigma_1^2 + \sigma_2^2 + \dots + \sigma_n^2)}}{n}\end{aligned}\tag{4.12}$$

based on the consideration that the error of the average magnitude estimate is characterized by a variance that is equal to the sum of the variances of the errors associated with the single-station errors, assuming independency of the errors, where n is the number of triggered stations.

If the error of each station has the same standard deviation, σ , Eq.4.12 assumes the well known expression:

$$\sigma_M = \frac{\sigma}{\sqrt{n}}\tag{4.13}$$

4.6.2. Location Uncertainty

Location error is defined as the scalar distance between the estimated location and the true network epicentral location. As more stations are triggered, the location estimate is updated producing a decrease in the location error.

The ElarmS tests on the 32 events pointed out that the location error stabilizes after 4 seconds.

The location error is modeled as lognormal distribution that is commonly used for probability distribution function of positive quantities such as the location error. The location error at 1 second represents the distance between the first triggered station and the epicenter, as the second station is triggered the epicenter is located between the two stations and so on, this implies that the location accuracy is dependent on the station density in the epicentral area.

At 3-4 seconds the error stabilizes, corresponding to 4 stations triggered.

The location error as a function of time is represented in the following figure.

The error in the epicentral distance estimate is related to the location error, the worst case has been considered that is represented by alignment of epicenter, predicted epicenter and target location.

In this case the epicentral distance error is represented by the location error.

Cases of epicenter mislocation have been observed and the main cause of large location error is noise.

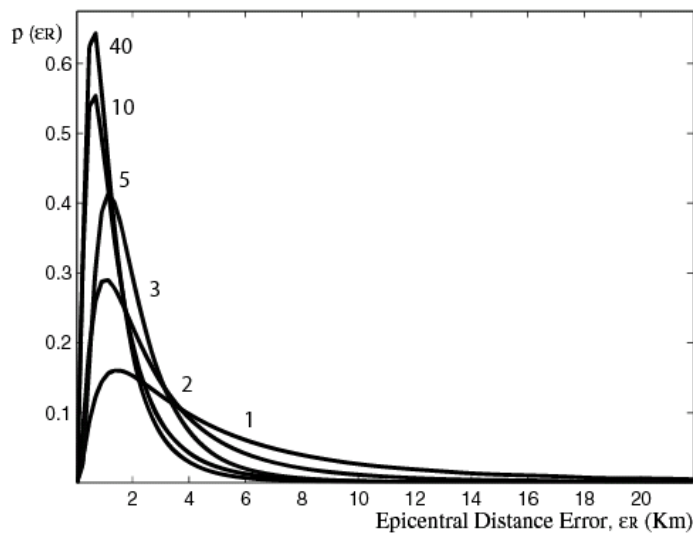


Figure 4.7 Location error (Km) distribution as a function of time, considering the zero time the instant when the first station is triggered.

T	μ	σ
1 s	1.41	1.02
2 s	0.83	0.88
3 s	0.59	0.66
4 s	0.37	0.75
5 s	0.19	0.83
6 s	0.15	0.82
7 s	0.075	0.76
8 s	0.06	0.76
9 s	0.06	0.76
10 s	0.07	0.76
11 s	0.07	0.76
12 s	0.07	0.76
13 s	0.07	0.76
14 s	0.09	0.79
15 s	0.09	0.79
20 s	0.09	0.79
25 s	0.09	0.79

Table 4.2 Epicentral distance error is characterized by mean, μ , and the standard deviation, σ , function of time.

4.6.3. Attenuation model uncertainty

The attenuation model error is the difference between the predicted peak ground acceleration (PGA), estimated with Eq. 4.14.

$$\log_{10} PGA = 0.7179M + 2N - N \log_{10}(R) - 3.2373 \quad 4.14$$

where M is the magnitude, R is the epicentral distance and N is a coefficient which is a function of the magnitude, defined by a look up table that relates N to M and the observed PGA recorded during the course of the earthquake.

The error in the attenuation relationship represents the error in the PGA prediction given the correct magnitude and distance. The attenuation relationship error follows a Gaussian distribution.

In the following figure is represented the model for the attenuation relationship error for the 32 events. The error distributions are similar for all the events, with means around zero, except for one which has a mean of 2.0. This is a M 3.1 earthquake that occurred 3/11/2000. For this event all

stations that recorded detectable ground shaking were with 10 km. The errors in the attenuation relations are greater at small epicentral distances and in this case predict a higher intensity of ground shaking than occurred. The errors for all events are combined to determine a single Gaussian error distribution for the attenuation relations. It has a mean of 0.26 and standard deviation equal to 0.9.

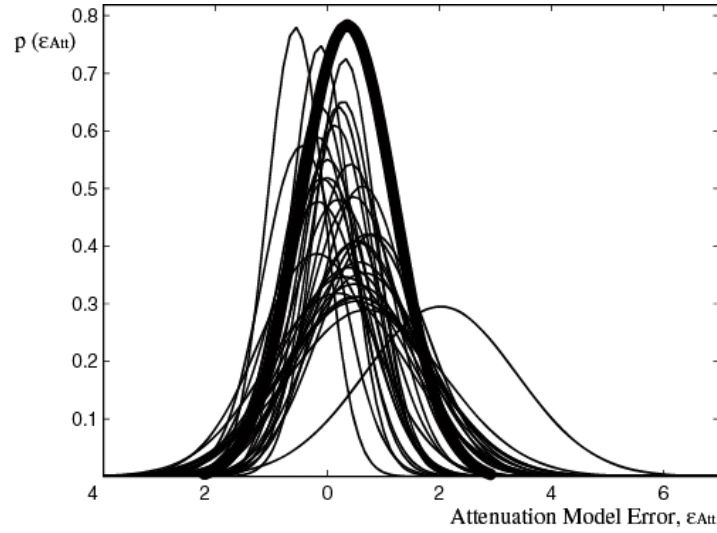


Figure 4.8 Attenuation model uncertainty for the 32 events, with thin black line, and the attenuation model error, for all data, with the thick black line.

A model for the attenuation relationship error is assumed considering all the events, represented by a Gaussian distribution with mean as 0.26 and standard deviation equal to 0.9.

4.6.4. Total Error

Error analysis represents a fundamental tool for estimating the error associated to the ground motion parameter, the single uncertainties are propagated through to the output, that is a function of the estimated magnitude, \hat{M} , and the estimated epicentral distance, \hat{R} :

$$PGA = f(\hat{M}, \hat{R}) \quad 4.15$$

where f represents ElarmS attenuation relationship Eq. 4.14 (Allen, 2004).

The predicted magnitude and epicentral distance are defined from the true true magnitude M , the true epicentral distance R , using their time dependent errors ε_M , ε_R respectively:

$$\begin{aligned} \hat{M} &= M + \varepsilon_M \\ \hat{R} &= R + \varepsilon_R \end{aligned} \quad 4.16$$

The error in the PGA prediction, ε_{PGA} , is determined by differencing the logarithm of the observed and the predicted PGA :

$$\varepsilon_{PGA} = \log(\hat{PGA}) - \log(PGA) = \log(f(M + \varepsilon_M, R + \varepsilon_R)) - \log(PGA) \quad 4.17$$

We use the difference in the logarithm of the PGA observation to account for the wide range of PGA values given the range of magnitudes for the dataset. This is typical in studies of ground shaking attenuation.

For every observation of magnitude and epicentral distance will be estimated the predicted magnitude and epicentral distance, \hat{M} and \hat{R} , according to Eq. 4.16

The Monte Carlo simulation consists in randomly choosing errors from their distributions to define the predicted magnitude and location, \hat{M} and \hat{R} from Eq. 4.16 and, based on these values the predicted ground motion parameter, \hat{PGA} is defined from Eq. 4.14.

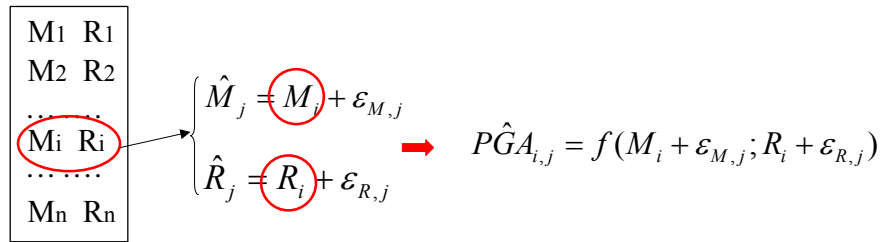


Figure 4.9 Monte Carlo simulation, prediction of ground motion parameter represented by \hat{PGA} , where for j is indicated the Monte Carlo cycle and for i the observation.

The predicted \hat{PGA} will be compared with the observed value of PGA and the error will be evaluated as the difference between prediction and observation, comparing $\log_e(\hat{PGA})$ to $\log_e(PGA)$.

The Monte Carlo simulation procedure is represented in the following figure.

Uncertainty propagation analysis has been carried out for different instants of time from 1 second to 25. For example for instant \bar{t} we have $\varepsilon_{tot}(\bar{t}) = f(\varepsilon_M(\bar{t}), \varepsilon_R(\bar{t}), \varepsilon_{IM})$ that is obtained from Monte Carlo simulation adopting the error models for ε_M and ε_R related to instant \bar{t} . This procedure will be adopted to build the pdf of the total error related to each 1 sec increment.

The uncertainty associated with the ground motion parameter prediction follows a Gaussian distribution with mean and standard deviation that vary with time.

The mean goes from a value of -0.61 for 1 second to a value of -0.17 at 5 seconds, finally assuming a value of 0.16 for 20 seconds.

The standard deviation decreases with time going from 1.33 at 1 second to 1.1 at 5 seconds to 1.16 at 20 seconds.

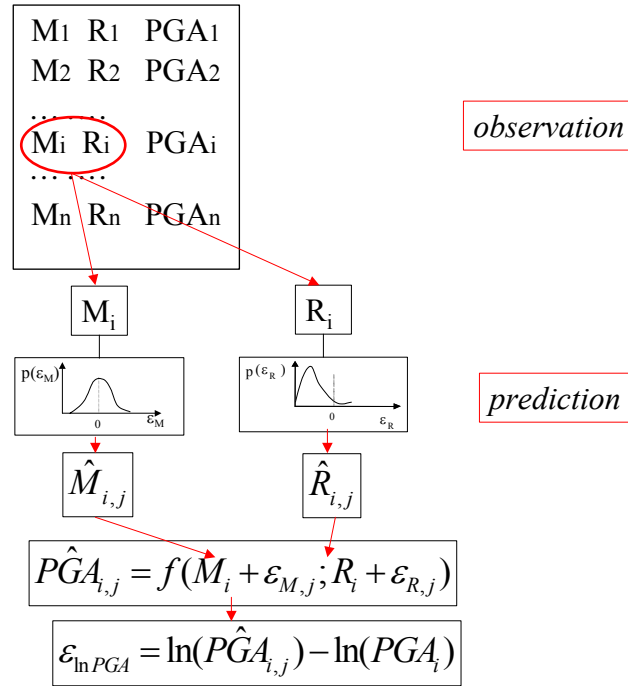


Figure 4.10 Monte Carlo simulation: for each observation i , M_i and R_i , and for each cycle j errors, ε_M and ε_R , are randomly chosen from their distributions to define the predicted $\hat{M}_{i,j}$, $\hat{R}_{i,j}$ and then $\hat{PGA}_{i,j}$ to be compared to the observed PGA_i , in order to define the distribution of the total error.

The values that characterize the error associated with the PGA prediction are described in the following table.

t	μ	σ	aad	rms
1 s	-0.61	1.33	1.15	1.5
5 s	-0.17	1.1	0.86	1.1
10 s	0.01	1.02	0.78	1.02
20 s	0.16	0.95	0.73	0.95
25 s	0.16	0.95	0.73	0.95

Table 4.3 The total uncertainty of the prediction is characterized by the mean, μ , the standard deviation, σ , the average absolute deviation, aad, and root mean squared, rms.

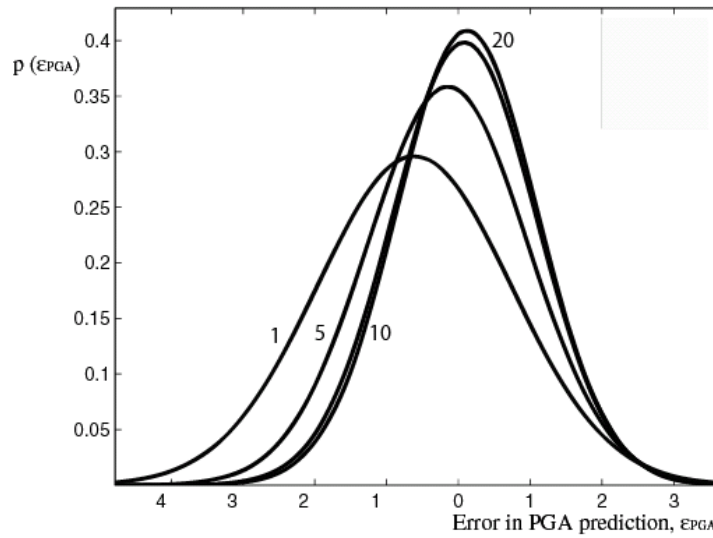


Figure 4.11 PGA error distribution, result of the uncertainty propagation, as a function of time, where zero time is the instant when the first station is triggered.

At this point in order to study the influence of the single error on the total error a sensitivity analysis has been carried out.

4.6.5. Sensitivity analysis

To determine the largest source of error in the PGA predictions we conduct a simple sensitivity analysis. The total error in the PGA prediction can be expressed as:

$$\varepsilon'_{PGA} = \log(f(M + \varepsilon_M, R + \varepsilon_R) + \varepsilon_{Att}) - \log(f(M, R)) \quad 4.18$$

In order to consider the influence of the single errors, different cases have been considered, the following table synthesizes the cases.

<i>Case</i>	ε_M	ε_R	$\varepsilon_{ATT.M.}$
1	X	X	X
2		X	X
3	X		X
4	X	X	

Table 4.4The cases considered are defined by different combinations of the errors.

We consider four cases (Grasso and Allen, 2005). In case 1 we include all three sources of error in equation 4.18. The characteristics of ε'_{PGA} are shown in Table 4.9. The errors are of course very similar to those in Table 4.4 where the total error was determined by differencing the prediction with the observed PGA. In case 2 we set the error in the magnitude estimate, ε_M , to zero thereby

assuming an exact magnitude is available for an event and ε_R and ε_{Att} are the only sources of error in ε'_{PGA} .

The following cases, from 2 to 4, have been designed in order to isolate and quantify the contribution of the single errors on the total error.

The Case 1, in which all the error are included, represents the reference point to which compare the results of the other cases. Comparing the results of the Case 1 obtained with synthetic data to the results obtained from the error defined as the difference between predictions and real data, is possible to confirm the perfect agreement of the results.

In Case 2 the magnitude error influence is evaluated, in the Case 3 the epicentral error is quantified and finally in Case 4 the attenuation model error influence is weighted.

The results related to Case 2 are synthesized in the following table.

<i>Case 2</i>				
t	μ	σ	aad	rms
1 s	0.076	0.93	0.74	0.93
5 s	0.18	0.9	0.73	0.92
10 s	0.19	0.9	0.73	0.92
20 s	0.19	0.9	0.73	0.92
25 s	0.19	0.9	0.73	0.92

Table 4.5 The Case 2 is characterized reporting the parameters describing the total error associated with the considered errors, ε_R and $\varepsilon_{ATT.M.}$.

Analysing the results of Case 2, we can notice that the magnitude error has some influence initially on the behaviour of the total error of Case 1. The magnitude has negative error, causing a negative value of the mean in Case 1, that does not happen in Case 2, in which the magnitude error equal to zero. Considering no magnitude uncertainty is possible to notice that the prediction is still characterized by an error that has a standard deviation equal to 0.9 for every instant of time considered, equal to the attenuation model error.

The mean of the error is equal to 0.18 at 5 seconds and 0.19 at 10, 20 and 25 seconds that is equal to the mean of the attenuation error. These considerations lead to the conclusion that with exact magnitude value the error is mainly due to the attenuation model error, except for the first second where location error is of some influence.

Magnitude error has an influence of some importance in the first second, while after 5 seconds the effect might be neglected.

Case 3, represents the case of correct epicenter location while magnitude and attenuation model are sources of errors, the results are reported in the following table.

<i>Case 3</i>				
t	μ	σ	aad	rms
1 s	-0.48	1.34	1.14	1.43
5 s	-0.15	1.125	0.9	1.13
10 s	0.03	1.06	0.8	1.06
20 s	0.2	0.99	0.8	1
25 s	0.2	0.99	0.8	1

Table 4.6 The Case 3 is characterized reporting the parameters describing the total error associated with the considered errors, ϵ_M and $\epsilon_{ATT.M.}$.

Observing the results of Case 3 is possible to confirm that the influence of the epicentral distance error on the total error is present only for the first second, while becomes not influent after 5 seconds. As is possible to notice from the comparison of the results of Case 3 and Case 1 in correspondance of the first second, the effect of the location error is only on the mean value, while the other parameters are not influenced.

In the case of location error equal to zero (Case 3), when the magnitude error goes to values close to zero, the contribution to the prediction error comes only from the attenuation model error, in this way the error never yields to zero values.

Finally Case 4 is considered in which the attenuation model error is equal to zero.

<i>Case 4</i>				
t	μ	σ	aad	rms
1 s	-0.91	1.03	1.13	1.38
5 s	-0.48	0.68	0.67	0.83
10 s	-0.3	0.56	0.51	0.64
20 s	-0.14	0.43	0.36	0.45
25 s	-0.14	0.43	0.36	0.45

Table 4.7 The Case 4 is characterized reporting the parameters describing the total error associated with the considered errors, ϵ_M and ϵ_R .

The most important contribution to prediction error is given by the attenuation model error as confirmed by the results of Case 4.

Is interesting to notice that the mean value goes to a value of -0.14 and the standard deviation reaches a value of 0.43 less than the values observed in the other cases. The influence of the attenuation model error is either on mean and on standard deviation for every instant of time considered.

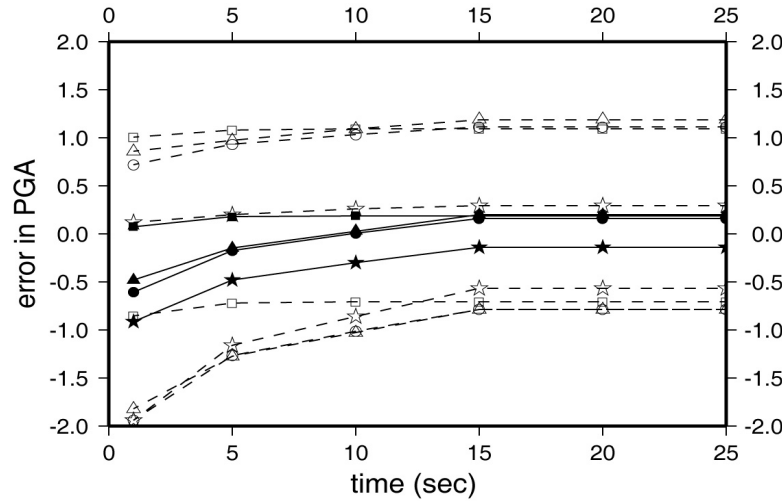


Figure 4.12 Error in PGA as a function of time for the four cases. The mean is shown as a solid symbol joined by a solid line, plus and minus one standard deviation are shown with open symbols joined by a dashed line. Case 1 (circles) includes all sources of error. Case 2 (squares) neglects error in the magnitude estimate, ε_M , but includes epicentral distance error, ε_R , and the attenuation relation error, ε_{Att} . Case 3 (triangles) neglects ε_R but includes ε_M and ε_{Att} . Case 4 (stars) neglects ε_{Att} but includes ε_M and ε_R .

	Case 1				Case 2				Case 3				Case 4			
	μ	σ	aad	rms	μ	σ	aad	rms	μ	σ	aad	rms	μ	σ	aad	rms
s	-0.66	1.37	1.2	1.52	0.076	0.93	0.74	0.93	-0.48	1.34	1.14	1.43	-0.91	1.03	1.13	1.38
s	-0.22	1.12	0.9	1.15	0.18	0.9	0.73	0.92	-0.15	1.125	0.9	1.13	-0.48	0.68	0.67	0.83
3 s	-0.04	1.06	0.85	1.06	0.19	0.9	0.73	0.92	0.03	1.06	0.8	1.06	-0.3	0.56	0.51	0.64
5 s	0.12	0.99	0.8	1	0.19	0.9	0.73	0.92	0.2	0.99	0.8	1	-0.14	0.43	0.36	0.45
3 s	0.12	0.99	0.8	1	0.19	0.9	0.73	0.92	0.2	0.99	0.8	1	-0.14	0.43	0.36	0.45
5 s	0.12	0.99	0.8	1	0.19	0.9	0.73	0.92	0.2	0.99	0.8	1	-0.14	0.43	0.36	0.45

Table 4.8 Distribution of errors in the predicted PGA using the ElarmS error model, ε_{PGA} . For each case the errors have a Gaussian distribution with mean, μ , the standard deviation, σ . The average absolute deviation, aad, and root mean squared, rms, of the errors are also shown. Case 1 is the total error in PGA which includes errors in the magnitude, ε_M , the epicentral distance, ε_R , and the attenuation relations, ε_{Att} . In Case 2 ε_M is set to zero and errors in ε_R and ε_{Att} only are considered. In Case 3 ε_R is set to zero, ε_M and ε_{Att} only are considered. In Case 4 ε_{Att} is set to zero, ε_M and ε_R only are considered.

In summary, ε_R has a negligible contribution to uncertainty in PGA predictions, ε_M contributes initially (the first 5-10 sec only), and ε_{Att} is the most significant source of error, particularly at later times after several stations have recorded P-wave arrivals and contribute to the magnitude estimate (Grasso and Allen, 2005).

Chapter 5

5. Aspects of Feasibility and Reliability of Seismic EWS

Main aspects involved in feasibility and reliability of an EWS application are:

- the amount of warning time
- the probability of making wrong decisions (false alarms and missed alarms)

that represent, respectively, timeliness and reliability, conflicting requirements of EWS.

These parameters strongly influence EWS impact and effectiveness on seismic risk reduction.

With respect to the first point, the time available to activate security measures is the time interval from the detection of P-waves in the epicentral area, and the arrival of S-waves in the area where the structure or facility is located. This time interval, T_w , defined by Eqs. 2.1 and 2.2, is a function of the reporting time, T_r , and the S-wave travel time, T_s . The warning time, to be considered adequate for the activation of a security measure, has to be greater than the time necessary for its activation.

As a function of the epicentral distance, the area of interest may be decomposed in homogeneous zones characterized by equal amount of warning time available. This analysis has been carried out for the San Francisco Bay area (Working Group '02) by Allen et al.

Although for a territorial feasibility assessment for each area has to be evaluated an estimate of expected annual probability of false alarm and missed alarm in order to have an overview of possible EWS applications.

Assuming that the warning time provided by the EWS is sufficient for security measure activation, EWS effectiveness is influenced by system reliability in terms of probability of making wrong decisions, fundamental aspect in a pre-installation feasibility assessment and for decision making during the course of the earthquake.

5.1. Probability of wrong decisions in a pre-installation scenario

When examining the feasibility of installing an EWS for a facility, it is important to have a mechanism to control the probabilities of false and missed alarms. Since the decision to activate the alarm is based on a predictor, \hat{IM} , false alarms can be caused by the predictor exceeding the warning threshold even though the actual intensity measure, IM , that occurs at the site does not reach the critical value. Similarly, missed alarms can be caused by the predictor not exceeding the warning threshold even though the actual intensity measure reaches its critical value.

For a given facility, the critical threshold, a , of IM may be chosen by the user as the value of IM for which damage (or high economic losses) is expected to occur with a high probability. However, to

control the probability of wrong decisions, the warning threshold is chosen as the product of the critical threshold a and a parameter, c , to be specified during the design process. The critical threshold depends on the facility, structure or equipment to be protected, but the warning threshold $c \cdot a$ depends on the design process chosen to optimize the warning system. The parameter c provides a mechanism to control the incidence of false and missed alarms. Note that it is not possible to simultaneously reduce both but c may be used to control the trade-off between them. A false alarm occurs when the EWS predicts a value, \hat{IM} , that exceeds the warning threshold, $c \cdot a$, while the actual value, IM , of the intensity measure at the site turns out to be less than the value of the critical threshold, a .

In a pre-installation scenario, the probability of false alarm is therefore given by:

$$P_{fa} = P[IM \leq a \mid \hat{IM} > c \cdot a] \quad 5.1$$

Similarly the probability of missed alarm is:

$$P_{ma} = P[IM > a \mid \hat{IM} \leq c \cdot a] \quad 5.2$$

The values of the probabilities of false and missed alarms, P_{fa} and P_{ma} , are an important tool for the decision-making process during pre-installation design and during operation in a seismic event.

During design, the anticipated rate of missed and false alarms represents a guideline for EWS feasibility. The realization of EWS could be feasible or not, depending on whether the requirements in terms of warning time available and the probability of wrong decisions can be met. A useful tool to evaluate an EWS may be constructed by using a seismic hazard map to provide the probability of exceedance of ground shaking intensity, given a site and time interval of interest, to produce a map of probability of wrong decisions. Such a map would help when performing a territorial feasibility assessment of EWS applications.

During a seismic event, the (automated) decision to activate protective measures may be done either by comparing the requirements in terms of warning time needed and the tolerable level of P_{fa} (or P_{ma}) based on the information made available by the EWS, or by monitoring a time-varying threshold $c(t) \cdot a$. This case is examined later in Chapter 7.

5.2. Procedure for estimating P_{fa} and P_{ma} in a pre-installation scenario

The main reasons for evaluating the probability of wrong decisions in a pre-installation scenario are to design the warning threshold, following the considerations presented before and, then to define the probabilities of false and missed alarms and their expected annual frequency that are tolerable to the owner or manager of the facility to be protected.

The probability of false or missed alarm, in a pre-installation scenario, can be evaluated as a time-independent variable, based on the seismicity of the area of interest. Time dependence could be neglected as a first approximation, assuming that the prediction uncertainty stabilizes after a certain time following the first trigger.

This simplified approach could be applied to special cases as Mexico City where the location of the fault area, the configuration of the seismic stations enable the possibility of assuming that the uncertainty of the prediction stabilizes after the first seconds. The time-invariant approach will be based on the consideration of error as a time independent parameter and we will consider a certain pdf for the total error related to a certain instant of time.

By estimating the probability of false alarm, before the earthquake, we are primarily trying to answer to the question: How would an EWS perform during earthquakes that might occur in the area of interest, in terms of a false (or missed) alarm rate?

Prior information can be expressed by using the hazard (rate) function (Kramer, 1996) that defines the mean rate per year of events with intensity measure exceeding a certain critical value, given a site of interest.

The hazard (rate) function provides the information related to the expected intensity measures, IM , for a given site and period of interest that represents the known parameter in Fig. 5.1; on the other hand the unknown quantity is represented by the predicted intensity measure, \hat{IM} , that is evaluated by adding prediction error, ε_{tot} , to the actual IM . The prediction error ε_{tot} is defined taking in account the errors related to the prediction of magnitude, M , epicentral distance, R , and the error of the ground motion attenuation model. In Fig. 5.1 is represented the relation between the IM and \hat{IM} that are related by the ε_{tot} , that includes ε_M , ε_R and ε_{IM} .

The simulated EWS prediction process of ground motion parameters goes backward from the known intensity measure value, IM , to the predicted value, \hat{IM} .

The aim is to describe the EWS behaviour for a given seismic event, represented by the correspondent value of intensity measure, given by the hazard function, and to define the probability of having false and missed alerts; considering all the possible events, the probability of wrong decisions is defined, given an area of interest and a period of time of interest (one year), for

all the expected events. The key to forecast the behaviour of the EWS and the predicted value, given the real value from the hazard function, is the prior knowledge of the errors that we committ predicting the intensity measure of interest, as a result of the uncertainty propagation of the errors. The uncertainty propagation, is based on the assumptions of time independence of the errors of the earthquake parameters prediction and of the uncertainty related to the attenuation model.

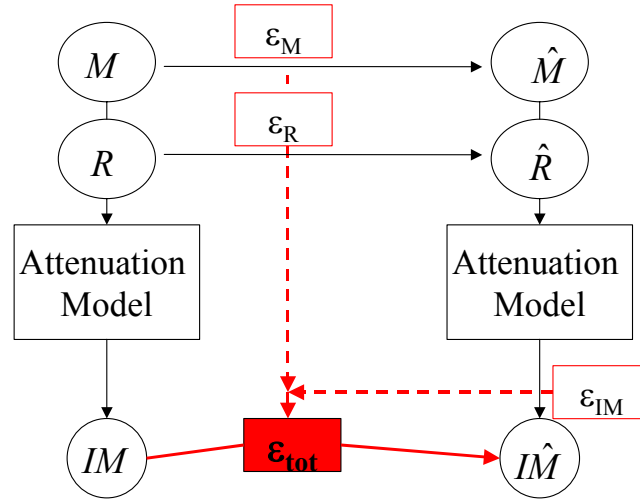


Figure 5.1 Simulation of the EWS process of prediction in a pre-installation analysis.

5.3. Prior information: Hazard function

The hazard (rate) function (Kramer, 1996) gives the mean annual rate of events with intensity measure exceeding a certain critical value, given a site of interest. From the mean rate, the probabily of exceedance of a critical value, given that an earthquake of interest has occurred, can be defined by considering the rate of exceedance rescaled by the rate corresponding to the minimum intensity measure of interest (cut-off value), called IM_0 , assuming a Poisson process for earthquakes:

$$\lambda(IM_c) = \lambda(IM_0) \cdot P[IM > IM_c | IM > IM_0] \quad 5.3$$

An exponential model is assumed for the hazard function for a site (but recall that the choice of IM used in the examples is \log_e PGA so this corresponds to a power law on PGA):

$$\lambda(IM) = k_0 10^{-k_1 IM} \quad 5.4$$

where k_0 and k_1 can be obtained by fitting the hazard function from a PSHA for the site. This model implies from Eq. 5.3 that (Grasso et al., 2005 a):

$$P[IM > IM_c | IM > IM_0] = 10^{-k_1(IM_c - IM_0)} \quad 5.5$$

The cumulative distribution function is then:

$$P[IM \leq IM_c | IM > IM_0] = 1 - 10^{-k_1(IM_c - IM_0)} \quad 5.6$$

and the expression for the PDF (probability density function) is derived by differentiating this cumulative distribution function:

$$p(IM | IM > IM_0) = k_1 \cdot \log_e 10 \cdot 10^{-k_1(IM - IM_0)} = \bar{c} \cdot 10^{-k_1 IM} \quad 5.7$$

where $\bar{c} = k_1 \cdot \log_e 10 \cdot 10^{k_1 IM_0}$.

In this work, the parameter k_I is estimated from a hazard function for the site of interest by using a minimum entropy criterion in which the relative entropy E is minimized with respect to k_I :

$$E = \sum_i p_i \log \left(\frac{p_i}{q_i} \right) \quad 5.8$$

where p_i represents the discrete probability distribution function derived from $p(IM | IM > IM_0)$ and q_i is the discrete probability distribution function derived from the given hazard function $\lambda(IM)$ using Eq. 12, so q_i is obtained by numerically differentiating the cumulative distribution function in the same way as $p(IM | IM > IM_0)$ was derived above. Therefore, p_i is a function of the parameter k_I but q_i is not. By minimizing the relative entropy, we determine the parameter k_I so that the model PDF is the best fit in an information-theoretic sense to the PDF implied by the hazard function for the site.

5.4. Probability of false alarm in a pre-installation scenario

The probability of false alarm, as defined in Eq.5.1, for Bayes rule can be expressed as:

$$\begin{aligned} P_{fa} &= P[IM \leq a | \hat{IM} > c \cdot a, IM > IM_0] \\ &= \frac{P[IM \leq a \cap \hat{IM} > c \cdot a | IM > IM_0]}{P[\hat{IM} > c \cdot a | IM > IM_0]} \end{aligned} \quad 5.9$$

where it is assumed that an earthquake of interest, i.e. $IM > IM_0$, has occurred and that $a > IM_0$.

The numerator, let us call it $P_{fa,1}$, is evaluated as:

$$P_{fa,1} = P \left[IM \leq a \cap \hat{IM} > c \cdot a \mid IM > IM_0 \right] \quad 5.10$$

$$= \int_{ca}^{\infty} \int_{IM_0}^a p(IM, \hat{IM} \mid IM > IM_0) dIM d\hat{IM}$$

which can be written, using Bayes rule, as:

$$P_{fa,1} = \int_{IM_0}^a \int_{ca}^{\infty} p(\hat{IM} \mid IM) \cdot p(IM \mid IM > IM_0) d\hat{IM} dIM \quad 5.11$$

where $p(IM \mid IM > IM_0)$ is given by Eq. 5.7 and $p(\hat{IM} \mid IM)$ is a Gaussian distribution with IM representing the mean value (if ε_{tot} has zero mean) and standard deviation σ_{tot} given by uncertainty propagation (Chapter 4). In the case that the prediction, \hat{IM} , is affected by a significant bias error (i.e. mean μ_{tot} of ε_{tot} is not close to zero), then the mean of the Gaussian distribution $p(\hat{IM} \mid IM)$ is $(IM \pm \mu_{tot})$ (from the definition of the prediction error as difference between prediction and observation). Substituting in Eq. 5.11:

$$P_{fa,1} = \int_{IM_0}^a \int_{ca}^{\infty} \frac{1}{\sigma_{tot} \sqrt{2\pi}} \exp \left[-\frac{1}{2} \left(\frac{\hat{IM} - IM}{\sigma_{tot}} \right)^2 \right] \cdot \bar{c} \cdot 10^{-k_1 IM} d\hat{IM} dIM \quad 5.12$$

The integral of the Gaussian distribution over \hat{IM} can be expressed in terms of the standard Gaussian cumulative distribution function Φ :

$$\int_{ca}^{\infty} \frac{1}{\sigma_{tot} \sqrt{2\pi}} \exp \left[-\frac{1}{2} \left(\frac{\hat{IM} - IM}{\sigma_{tot}} \right)^2 \right] d\hat{IM} = \Phi \left(-\frac{ca - IM}{\sigma_{tot}} \right) \quad 5.13$$

so Eq. 5.11 can be cast in a simpler form:

$$P_{fa,1} = \int_{IM_0}^a \Phi \left(-\frac{ca - IM}{\sigma_{tot}} \right) \cdot \bar{c} \cdot 10^{-k_1 IM} dIM \quad 5.14$$

The denominator of P_{fa} in Eq. 5.9 is expressed as:

$$P_{fa,2} = \int_{ca}^{\infty} p(\hat{IM} | IM > IM_0) d\hat{IM} \quad 5.15$$

which can be written, using the theorem of total probability, as:

$$P_{fa,2} = \int_{IM_0}^{\infty} \int_{ca}^{\infty} p(\hat{IM} | IM) \cdot p(IM | IM > IM_0) d\hat{IM} dIM \quad 5.16$$

This can be expressed in terms of the standard Gaussian cumulative distribution function Φ as:

$$P_{fa,2} = \int_{IM_0}^{\infty} \Phi\left(-\frac{ca - IM}{\sigma_{tot}}\right) \cdot \bar{c} \cdot 10^{-k_1 IM} dIM \quad 5.17$$

Summarizing, the probability of false alarm in a pre-installation analysis is given by (Grasso et al. 2005 a):

$$P_{fa} = \frac{\int_{IM_0}^a \Phi\left(-\frac{ca - IM}{\sigma_{tot}}\right) \cdot 10^{-k_1 IM} dIM}{\int_{IM_0}^{\infty} \Phi\left(-\frac{ca - IM}{\sigma_{tot}}\right) \cdot 10^{-k_1 IM} dIM} \quad 5.18$$

The integrals in the denominator and numerator here can be evaluated numerically for different values of c , given the value of a ; then curves of P_{fa} versus c can be plotted for different critical thresholds a . Examples are given later in Chapter 6.

5.5. Probability of missed alarm in a pre-installation scenario

The probability of missed alarms, as defined in Eq.5.2, can be written using Bayes rule as:

$$\begin{aligned}
P_{ma} &= P\left[IM > a \mid \hat{IM} \leq c \cdot a, IM > IM_0\right] \\
&= \frac{P\left[IM > a \cap \hat{IM} \leq c \cdot a \mid IM > IM_0\right]}{P\left[\hat{IM} \leq c \cdot a \mid IM > IM_0\right]}
\end{aligned} \tag{5.19}$$

where once again it is assumed that an earthquake of interest has occurred and that $a > IM_0$. The numerator can be expressed as:

$$\begin{aligned}
P_{ma,1} &= P\left[IM > a \cap \hat{IM} \leq c \cdot a \mid IM > IM_0\right] \\
&= \int_{-\infty}^{ca} \int_a^{\infty} p(IM, \hat{IM} \mid IM > IM_0) dIM d\hat{IM}
\end{aligned} \tag{5.20}$$

which can be written, using Bayes rule, as:

$$P_{ma,1} = \int_a^{ca} \int_{-\infty}^{\infty} p(\hat{IM} \mid IM) \cdot p(IM \mid IM > IM_0) d\hat{IM} dIM \tag{5.21}$$

where $p(IM \mid IM > IM_0)$ is given by Eq. 5.7 and $p(\hat{IM} \mid IM)$ is a Gaussian distribution as before (see after Eq. 5.11). Substituting in Eq. 5.21:

$$P_{ma,1} = \int_a^{ca} \int_{-\infty}^{\infty} \frac{1}{\sigma_{tot} \sqrt{2\pi}} \exp\left[-\frac{1}{2} \left(\frac{\hat{IM} - IM}{\sigma_{tot}}\right)^2\right] \cdot \bar{c} \cdot 10^{-k_1 IM} d\hat{IM} dIM \tag{5.22}$$

The integral of the Gaussian distribution over \hat{IM} can be expressed in terms of the standard Gaussian cumulative distribution function Φ :

$$\int_{-\infty}^{ca} \frac{1}{\sigma_{tot} \sqrt{2\pi}} \exp\left[-\frac{1}{2} \left(\frac{\hat{IM} - IM}{\sigma_{tot}}\right)^2\right] d\hat{IM} = \Phi\left(\frac{ca - IM}{\sigma_{tot}}\right) \tag{5.23}$$

so Eq. 5.22 can be cast in a simpler form:

$$P_{ma,1} = \int_a^{\infty} \Phi\left(\frac{ca - IM}{\sigma_{tot}}\right) \cdot \bar{c} \cdot 10^{-k_1 IM} dIM \tag{5.24}$$

The denominator of P_{ma} in Eq. 5.19 is:

$$P_{ma,2} = \int_{-\infty}^{ca} p(\hat{IM} | IM > IM_0) d\hat{IM} \quad 5.25$$

which can be expressed, using the theorem of total probability, as:

$$P_{ma,2} = \int_{IM_0}^{\infty} \int_{-\infty}^{ca} p(\hat{IM} | IM) \cdot p(IM | IM > IM_0) d\hat{IM} dIM \quad 5.26$$

This can be expressed in terms of the standard Gaussian cumulative distribution function:

$$P_{ma,2} = \int_{IM_0}^{\infty} \Phi\left(\frac{ca - IM}{\sigma_{tot}}\right) \cdot \bar{c} \cdot 10^{-k_1 IM} dIM \quad 5.27$$

The probability of missed alarms in a pre-installation analysis is therefore given by (Grasso et al. 2005 a):

$$P_{ma} = \frac{\int_a^{\infty} \Phi\left(\frac{ca - IM}{\sigma_{tot}}\right) \cdot 10^{-k_1 IM} dIM}{\int_{IM_0}^{\infty} \Phi\left(\frac{ca - IM}{\sigma_{tot}}\right) \cdot 10^{-k_1 IM} dIM} \quad 5.28$$

Chapter 6

6. Warning threshold design and Feasibility assessment

6.1. *Designing the test procedure: warning threshold setting*

The warning threshold is the EWS parameter that most influences the consequences impact of a decision this is the reason why accuracy and attention is needed for threshold design procedure. Two performance-based methods are described for warning threshold design. The first method is based on the operating characteristic (OC) function and the second one on cost-benefit considerations.

A test procedure leading to the acceptance/rejection of a hypothesis is simply a rule specifying whenever the hypothesis should be accepted or rejected based on the observed data. In our case accepting/rejecting the hypothesis means raising the alarm or doing nothing.

Designing a test procedure, can be defined by subdividing the sample space of all possible values that the predictor can assume, in two exclusive regions (Wald, 1947).

The space of all the possible samples is divided in:

- Region 1, for which acceptance of the hypothesis is preferred
- Region 2, is the critical region, for which rejection of the hypothesis is preferred

Considering the hypothesis of threshold exceedance, the critical region (2) is represented by all the values of intensity measure for which the alarm has to be activated and region 1 where the alarm has not to be activated.

The critical region is defined by the critical threshold, that is a given design parameter, provided by the user, representing the occurrence of structural damage or heavy economic losses.

The warning threshold corresponds to raising the alarm.

The warning threshold is defined by a decision criteria, based on user's requirements, that could be based on tolerable level of probability of wrong decision or on cost-benefit considerations.

The process of warning threshold design is described for both the situations, in which the constraints are related to tolerable level of wrong decision rate, in the first case, and to cost-benefit analysis, in the other case.

The test is designed defining the critical regions, by assigning the alarm threshold c_a that satisfies the user's requirements.

6.2. Threshold setting based on OC function

In the case that the user's requirements are given as the tolerable values of probabilities of false and missed alarms, the test procedure can be designed as follows.

The goal is to design a test that satisfies the conditions imposed on P_{fa} (or P_{ma}) by controlling the alarm threshold $c \cdot a$ on \hat{IM} . If the probability of false alarms is lowered, then the probability of missed alarms is increased. To design the alarm threshold for IM , the trade-off between P_{fa} and P_{ma} must be studied. Because of this trade-off, there is a limit as to how much the probabilities of wrong decisions can be reduced. This limit can be studied by using Stein's lemma, which states:

If a large number N of observations is available, then as $P_{ma} \rightarrow 0$, $P_{fa} \rightarrow \exp[-N K(p_0, p_1)]$

where K is the relative entropy (Kullback-Leibler distance):

$$K(p_0, p_1) = \int p_1 \log_e \frac{p_1}{p_0} dIM \quad 6.1$$

where p_0 is the PDF of IM conditioned on $\hat{IM} \leq c \cdot a$ (null hypothesis) and p_1 is the PDF of IM conditioned on $\hat{IM} > c \cdot a$.

Based on the user's specifications of tolerable P_{ma} , the corresponding P_{fa} is given by Stein's Lemma. By means of the operating characteristic (OC) function, the warning threshold can be defined. The OC function represents the probability of acceptance of the null hypothesis which corresponds to the probability of no alarm activation.

The ideal test corresponds to the ideal OC function shown in Figure 6.1, which gives a probability of acceptance of 1 for $IM \leq a$ when $\hat{IM} \leq c \cdot a$ (in acceptance zone) and probability of acceptance of zero for $IM \leq a$ when $\hat{IM} > c \cdot a$ (in the rejection zone). Note that the probability of acceptance conditioned on the predictor, \hat{IM} , may be written as $P[IM \leq a | \hat{IM}]$, that corresponds to P_{fa} in the rejection (critical) zone and $(1 - P_{ma})$ in the acceptance zone.

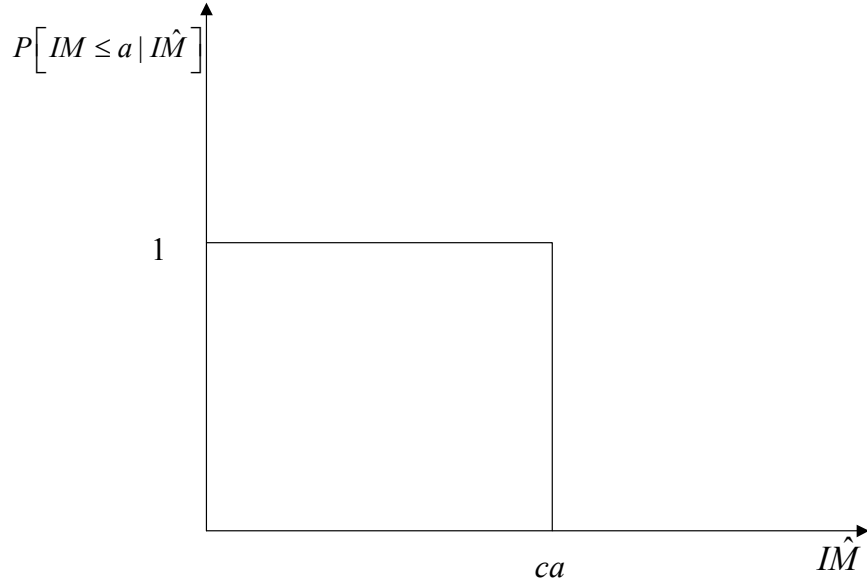


Figure 6.1 The ideal OC function

Based on uncertainties in the prediction of IM by \hat{IM} , which is based on the first seconds of observation of the seismic data, we cannot obtain an ideal OC function and we have to accept errors of type I and II (missed and false alarms). If the tolerable probability of a missed alarm in the acceptance zone is α and the tolerable probability of false alarm is β in the rejection zone, then the OC function will be characterized as in Figure 6.2 where β (or α) is the design requirement specified by the user and α (or β), respectively, is given by Stein's Lemma. The test is better designed if the OC function corresponding to the test is closer to the optimal OC function represented in Figure 5.

A prior definition of a possible set of thresholds, $c \cdot a$, can be defined and for each value of a the optimal OC function is defined. The discrete OC function representing the test may be evaluated at a finite number of points representative of the values of probabilities of wrong decisions for a range of values of $c \cdot a$ of interest. A best fitting curve can be constructed based on these points and the corresponding value of $c \cdot a$ will be the optimal warning threshold.

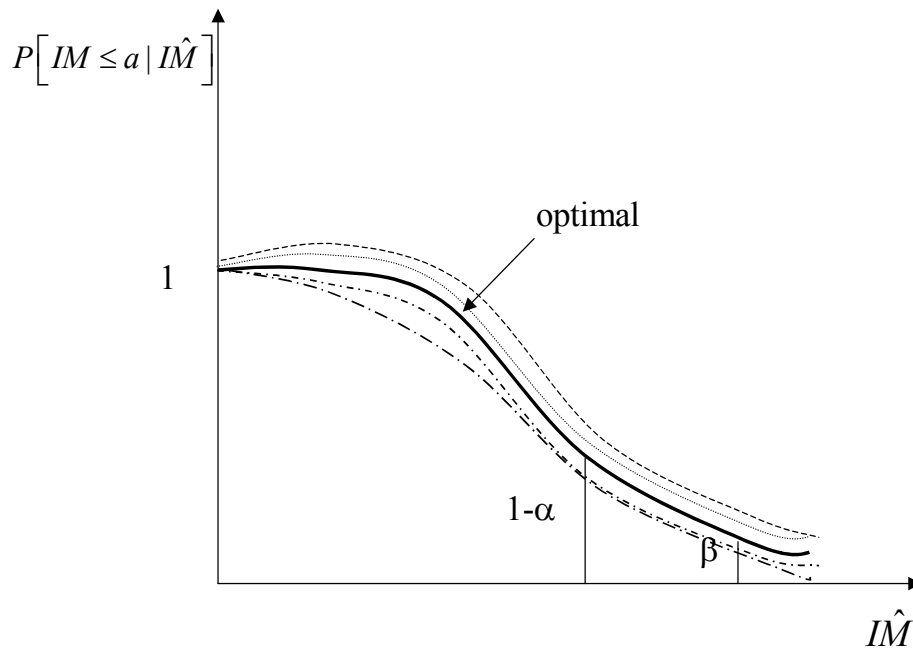


Figure 6.2 The optimal OC function

6.3. Threshold setting based on cost-benefit considerations

Specifying tolerable probabilities of wrong decisions, representing the design requirements for threshold setting, is often out of reach. In the collective imaginary and in most of the applications controlling the effects is more natural. The design constraint may be more easily linked to the cost of the effects that could derive from the decision taken, raising the alarm or doing nothing, instead of specifying tolerable probabilities of making wrong decisions.

Instead of applying an abstract decision criteria, often is more reliable a decision based on simple considerations coming from cost-benefit analysis over the two possible actions of raising the alarm or doing nothing.

The decision rule may be taken to be the minimization of the expected consequences.

A cost benefit analysis is described in detail in the table 6.1.

Action	Case: IM<a	Case: IM>a
Raise Alarm	False alarm: C _{fa}	Good Alarm: C _{ga}
No Alarm	Good Missed Alarm: C _{gm}	Missed Alarm: C _{ma}

Table 6.1 Cost benefit analysis for threshold design

Where:

$$\begin{aligned}
C_{ga} &= C_{eq} - C_{save} \\
C_{ma} &= C_{eq} \\
C_{gm} &\approx 0 \\
P_{ga} &= 1 - P_{fa} \\
P_{gm} &= 1 - P_{ma}
\end{aligned} \tag{6.2}$$

Where C_{eq} represents the expected costs due to the earthquake, C_{save} the expected savings as a consequence of the security measure activation, C_{fa} is the cost of a false alarm and C_{ma} is the cost of a missed alarm.

In the case we decide to raise the alarm, the expected cost is represented by:

$$\begin{aligned}
E[\text{cost} | \text{alarm}] &= C_{fa} \cdot P_{fa} + C_{ga} \cdot P_{ga} \\
&= C_{fa} \cdot P_{fa} + (C_{eq} - C_{save}) \cdot (1 - P_{fa})
\end{aligned} \tag{6.3}$$

In the case we decide not to raise the alarm, the expected cost is defined by:

$$\begin{aligned}
E[\text{cost} | \text{no-alarm}] &= C_{gm} \cdot P_{gm} + C_{ma} \cdot P_{ma} \\
&= C_{ma} \cdot P_{ma}
\end{aligned} \tag{6.4}$$

The decision criteria for deciding between the options, raising the alarm or not, is represented by the minimum cost rule:

Raise the alarm if and only if:

$$E[\text{cost} | \text{no-alarm}] \geq E[\text{cost} | \text{alarm}] \tag{6.5}$$

$$\begin{aligned}
C_{eq} \cdot P_{ma} &\geq C_{fa} \cdot P_{fa} + (C_{eq} - C_{save}) \cdot (1 - P_{fa}) \\
&= (C_{save} + C_{fa} - C_{eq}) \cdot P_{fa} + (C_{eq} - C_{save})
\end{aligned} \tag{6.6}$$

Eq. 6.6 can be taken as an equality used to select an appropriate value of c , solving the equation for P_{fa} (or P_{ma}). The tolerable value of P_{ma} (P_{fa}) may then be determined from Eq. 5.33 (or Eq. 5.21) for this value of c .

The tolerable value of P_{fa} (or P_{ma}) may be used for:

- evaluate the warning threshold, when the time-invariant approach is applicable
- alarm activation during the event while monitoring the P_{fa} (or P_{ma}), when the time invariant approach is not applicable

In order to evaluate the warning threshold assuming that the time invariant approach is applicable, (σ_{tot} in Eq. 5.18 and 5.28 is time invariant) the first step is to calculate the P_{fa} (or P_{ma}) given by Eq. 5.21 and 5.33 for a range of interest of values of warning threshold, given the value of critical threshold, a , that is a design data given from the user.

Then defined a curve that represents the P_{fa} (or P_{ma}) as a function of $c \cdot a$ we can evaluate the value of $c \cdot a$ that corresponds to P_{fa} (or P_{ma}) equal to the tolerable level β (α) evaluated in Eq. 6.6.

During a seismic event, however, more and more information becomes available to the EWS and so σ_{tot} will decrease with time. A refined analysis using a time-dependent warning threshold, $c(t)a$, would then be more appropriate. Alternatively, the probability of false and missed alarms could be monitored as a function of time and then the alarm would be raised when the tolerable level of probability of $P_{fa}(t)$ or $P_{ma}(t)$ is exceeded.

In the next chapter, we consider a refined decision-making procedure that is appropriate during a seismic event and which takes into account that the quality of the *IM* prediction improves as more and more information is obtained by the EWS. It is shown in Chapter 7 that in this case: $P_{fa}(t) + P_{ma}(t) = 1$, so Eq. 6.6 implies that the probability of a false alarm is tolerable if and only if:

$$P_{fa}(t) \leq \beta = \frac{C_{save}}{C_{fa} + C_{save}} \tag{6.7}$$

Similarly, since the alarm is not raised if and only if:

$$C_{eq} \cdot P_{ma} < (C_{save} + C_{fa} - C_{eq}) \cdot P_{fa} + (C_{eq} - C_{save}) \tag{6.8}$$

it follows that the probability of a missed alarm is tolerable if and only if:

$$P_{ma}(t) < \alpha = \frac{C_{fa}}{C_{fa} + C_{save}} \quad 6.9$$

It is clear from Eq. 6.7 and 6.9 that in this case, where the decision criterion is based on a cost-benefit analysis, $\alpha + \beta = 1$, which directly exhibits the trade-off between the threshold probabilities that are tolerable for false and missed alarms. If the threshold β is reduced to make false alarms less likely, then the threshold α for missed alarms becomes correspondingly larger.

6.4. Threshold design and Feasibility assessment: an example for Southern California

In the hypothesis of a future realization of an EWS for the protection of Southern California, in this section will be addressed a feasibility assessment of the application of interest of the potential end-user of the EWS (Grasso et al. 2005 a).

In particular we will be answering to the question: How would an EWS perform during earthquakes that might occur in the area of interest, in terms of false and missed alarm rate?

We might quantify the effectiveness of the EWS application, by providing to the end-user of the EWS the probabilities of wrong decisions to see whether they are acceptable or not and on the other hand we will be able to set the warning threshold in order to match the user's requirements.

In case of existing EWS application we might be interested in assessing the reliability of the system in terms of probabilities of making wrong decisions. The values of critical and warning threshold for an existing application are known parameters. For the given facility we can build the curves representing P_{fa} and P_{ma} as a function of the warning threshold ca (Eq. 5.18 and 5.28). We will be able to define the probabilities of wrong decisions related to the critical threshold and warning threshold that define the existing application. We could discover that the tolerable levels of incidence of false or missed alarms are not met. Based on the tolerable level of probability of wrong decisions we will be able to adjust the warning threshold, if time-invariant approach is applicable.

Assuming to be interested in Southern California, based on the Hazard function provided for the area of Los Angeles, we will evaluate the probabilities of wrong decision as a function of the warning coefficient, c . Assuming to know the critical threshold, a , provided by the user, the warning threshold will be set based on the design requirements in case of new EWS application (if time-invariant approach is applicable).

In case of existing application, given the value of the critical threshold, a , and the warning threshold, ca , the performance and feasibility assessment of the EWS application will be carried out by evaluating the corresponding expected annual probabilities of wrong decisions (Eq. 5.18 and

5.28). If the annual probabilities of wrong decision result not acceptable the warning threshold will be set in order to match the tolerable levels (assuming that the time-invariant approach is applicable).

Cua and Heaton prediction method is choosen as the earthquake predictive model (M_1 in the Fig.4.3) of interest, the attenuation model used (M_2 in Fig.4.3) is the Cua and Heaton relation and the intensity measure parameter of interest provided in output is the peak ground acceleration in \log_{10} scale (Eq. 2.11).

The parameters a, b, d, e , in Eq. 2.11 are defined by Cua and Heaton (2004) for different soil types. Rock type has been considered, where:

$$a = 0.779; b = 2.55 \cdot 10^{-3}; d = 1.352; e = -0.645; \varepsilon = \text{Gaussian}(0, 0.243).$$

The intensity measure IM is the peak ground acceleration (PGA) on a \log_{10} scale. The chosen hazard function for the Los Angeles area is shown in the following figure and it represents the mean rate of exceedance versus PGA in g units. The hazard function is fitted, as described previously, by using a minimum relative entropy criterion in order to define the coefficient k_I to describe the probability distribution function of IM . Minimizing the relative entropy, a value of $k_I=1.06$ is obtained.

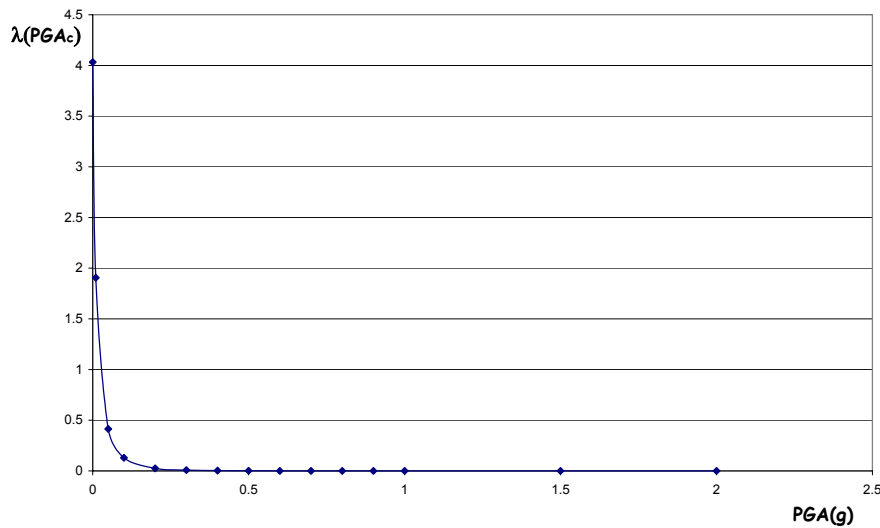


Figure 6.3 Hazard function for Los Angeles representing the annual probability of exceedance of PGA.

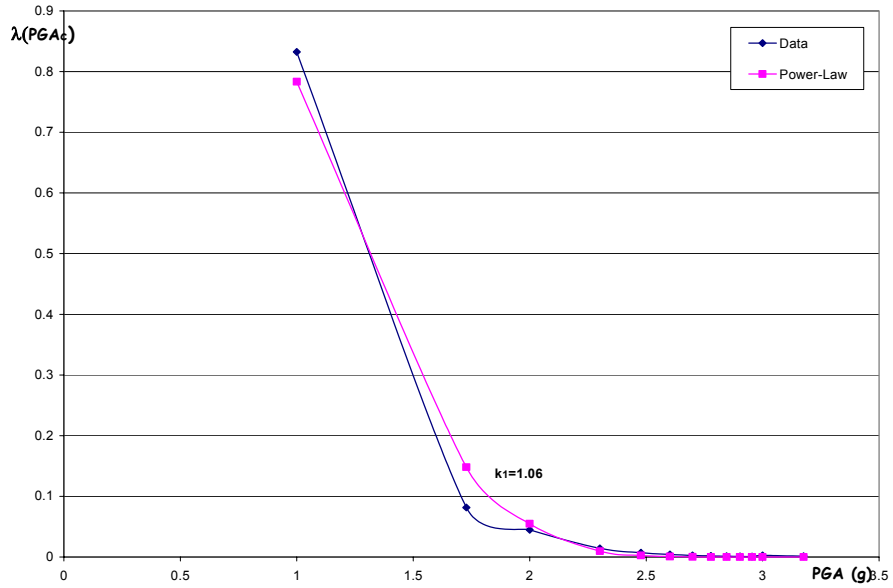


Figure 6.4 Fitting the Hazard function for Los Angeles with power-law

In order to simulate the behaviour of the EWS, in the prediction process we need to know the total error associated to the process, defined in the uncertainty propagation analysis.

In uncertainty propagation based on the assumption of time independency of the errors, will be chosen:

- ε_M : Gaussian (0, 0.5)
- ε_R : ignored at this stage
- ε_{IM} : Gaussian (0, 0.243)

correspondent to the error pdf of magnitude at 4 sec (Cua and Heaton, 2004) and for the attenuation model error, respectively, neglecting at this stage the epicentral distance error.

The total error associated to the predicted \hat{IM} , is defined as described in Chapter 4 (uncertainty propagation):

- ε_{tot} : Gaussian (0, 0.44)

Modeling the total error associated with the prediction is fundamental step for evaluating the consequences of a making wrong decision.

The probabilities of false and missed alarm are evaluated based on the Eq.5.18 and 5.28 as a function of the warning threshold factor, c , for different values of the critical threshold, a . Notice that for P_{fa} in the approximate range of 0.05 to 0.4, the choice of c is insensitive to a .

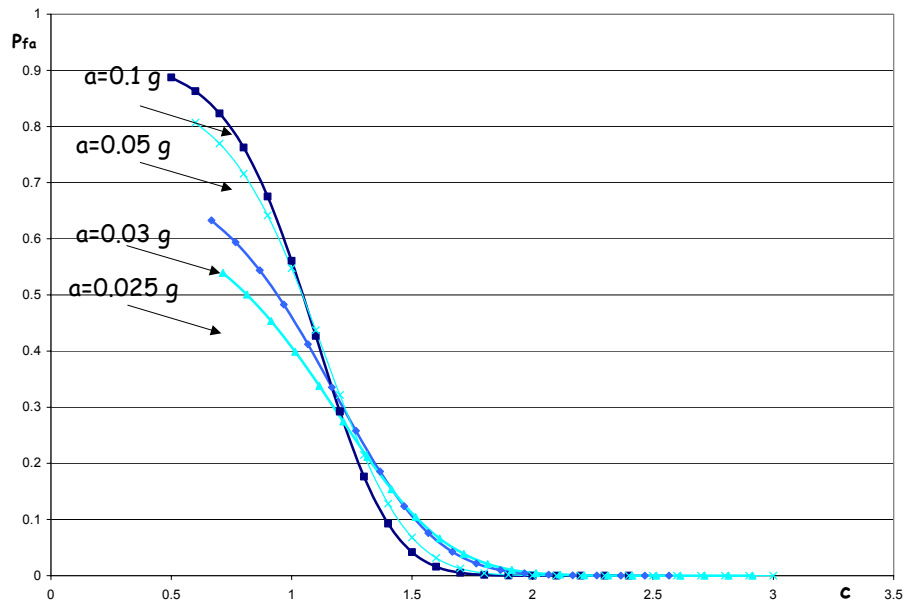


Figure 6.5 Probability of false alarm as a function of warning threshold factor c for different critical thresholds, a , expressed in g's.

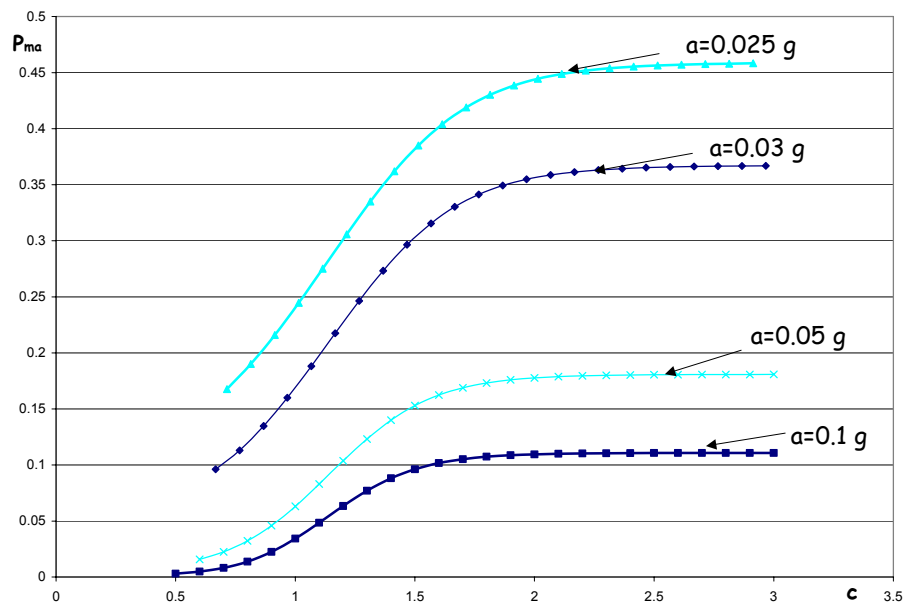


Figure 6.6 Probability of missed alarm as a function of warning threshold factor c for different critical thresholds, a , expressed in g's.

if it is false alarms that the the user is most concerned about, the warning threshold will be set so that the tolerable level of false alarm will not be exceeded.

If the tolerable level of probability of false alarm is equal to 0.4, given the critical threshold equal to 2 cm/s/s, the warning threshold will be set equal to 2.22 (Fig. 6.7).

From Fig. 6.8 assuming the warning threshold equal to 2.22 and given the critical threshold equal to 2 cm/s/s, we will obtain a P_{ma} of 0.045, that has to be accepted .

If this value of P_{ma} is not acceptable (tolerable level is exceeded) the warning threshold value has to be redesigned iteratively till the requirements are matched.

The graphs of P_{fa} (or P_{ma}) vs. the warning threshold factor, c , are useful, in the case of existing application, for performance and feasibility assessment of the EWS application. For example in the case of $a = ca = 2 \text{ cm/s/s}$ the corresponding P_{fa} is 0.8 and P_{ma} is 0.025 (from Fig. 6.7 and 6.8). assuming that the user is concerned on false alerts and from the cost-benefit analysis comes out that the tolerable level of P_{fa} is equal to 0.4, the threshold settings result inadequate. Is important to point out that P_{fa} and P_{ma} are parameters that can be controlled.

We will use again the graphs in Fig. 6.7 and 6.8 assuming $P_{fa} = \beta = 0.4$. Based on this requirement we will be able to redesign the warning threshold in order to match the requirements, assuming time-invariant approach is applicable.

The warning threshold corresponding to the condition $P_{fa} = \beta = 0.4$ is equal to 2.2 cm/s/s. Due to the trade-off between false and missed alerts the P_{ma} value increased from a value of 0.025 to a value of 0.42. Can we accept this value of P_{ma} ? If the answer is positive the process ends accepting the “new” warning threshold. If not we have to iterate the process several times until the conditions on P_{fa} and P_{ma} are met. Fig. 6.9 visualizes the trade-off between P_{fa} and P_{ma} .

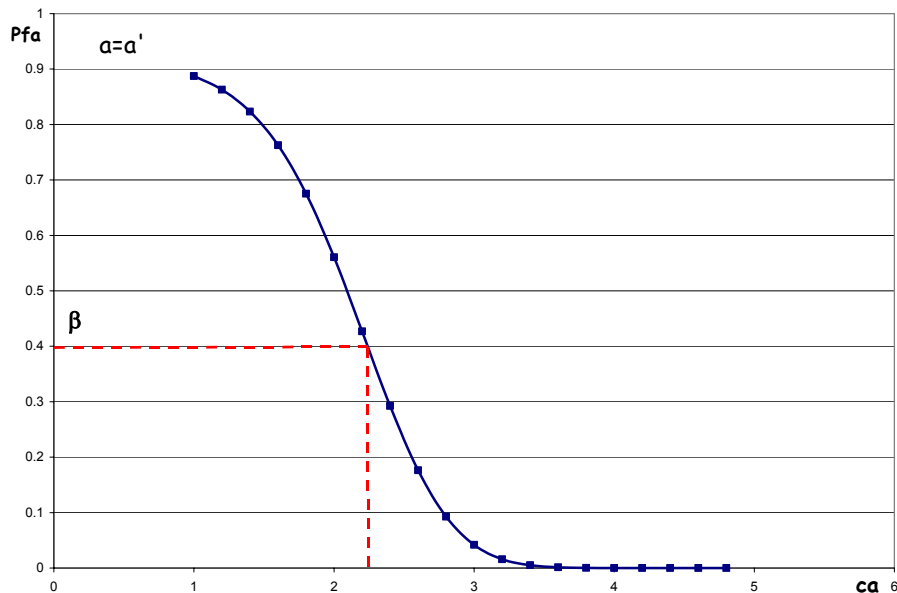


Figure 6.7 The curve represents the probability of false alarm for a given critical threshold a' equal to 2 cm/s/s, as a function of the warning threshold. Defined the tolerable value of probability of false alarm, as described above, is possible to define the correspondent warning threshold.

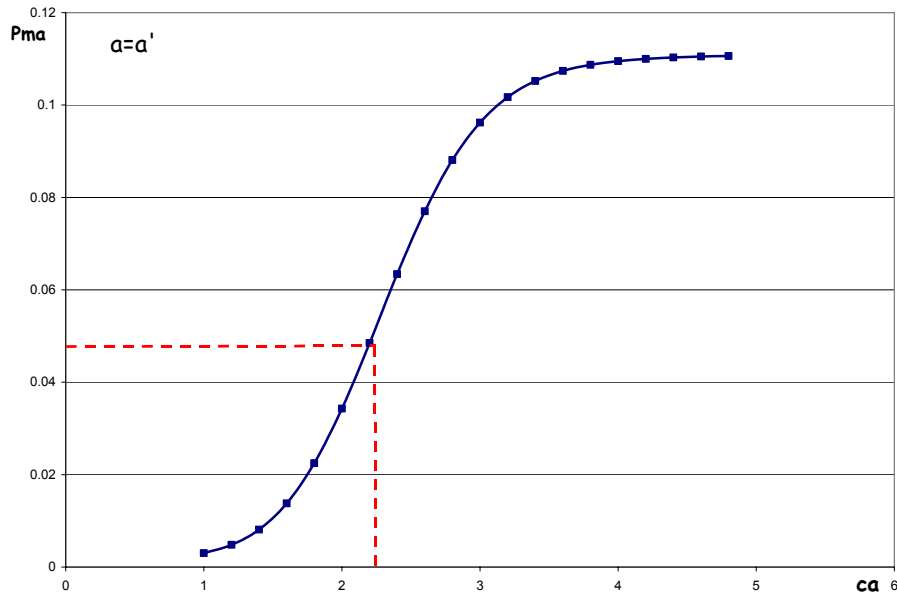


Figure 6.8 The curve represents the probability of missed alarm for a given critical threshold a' equal to 2 cm/s/s, as a function of the warning threshold. Defined the tolerable value of warning threshold as described above, is possible to define the correspondent probability of missed alarm to be accepted.

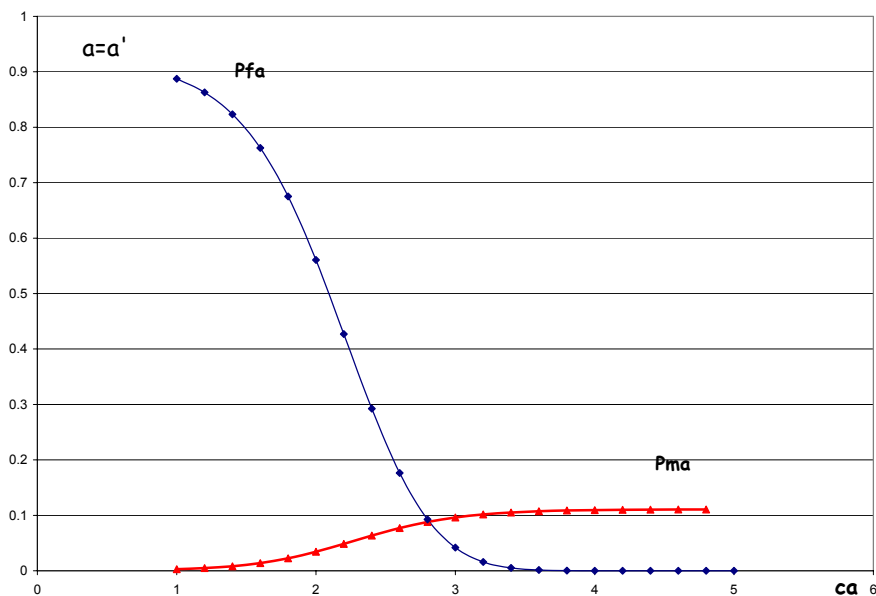


Figure 6.9 The curve represent the probability of false (blue line) and missed alarm (red line) as a function of the warning threshold. This graph visualizes the trade-off between probability of false and missed alarm, decreasing the tolerable level of probability of false alarm we will have as a consequence an increase of probability of missed alarm that we will have to accept.

On the other hand the curves represented in Fig. 6.5 and 6.6 will give a sense of the feasible applications representing the probabilities of false and missed alarm for a given area of interest. In this way is possible to map and decompose the areas surrounding the epicentral one in homogeneous areas that will be characterized by a certain amount of warning time and an expected

probability of wrong decision. Based on this information for each area of interest it will be possible to assess the feasible EWS applications.

Chapter 7

7. Operational aspects of EWS: Decision making

7.1. Sequential test

During the seismic event we have to decide between the two options: raise the alarm, do nothing. This decision is based on a parameter, the so called predictor. The decision problem may be approached by the theory of hypothesis testing (Wald 1947). The sequential method of testing an hypothesis may be described as follows. A rule is given for making one of the following three decisions during the course of the seismic event:

- Accept the hypothesis
- Reject the hypothesis
- Continue and make an additional observation.

Such a test is carried out sequentially. On the basis of the first observation a decision is made. In the case the first option is chosen (accept) the process is ended, if the second or third decision (reject or continue) is made a second observation is made. Again on the basis of the first two observations a decision is made. If the second or third decision is made a third trial is made and so on. The process is carried out till one of the first decisions is made. The number of observations is a random number depending on the outcome of the observations.

In our case the decision is made based on the observation of the predictor that represents the outcome of the prediction process of the EWS. A rule for making one of the three decisions consists in defining the critical region. For each observation the hypothesis will be accepted or rejected if the observation lies in the critical region or not. At every trial the observation will be drawn and compared with the critical region. Lets consider an example of sequential test. The case is of a lot of manufactured products that has to be accepted or rejected depending on the outcome of the inspection. Each product may be considered defective or non-defective and the lot will be accepted if the probability of defectives in the lot is less or equal than a given value p' , that corresponds to a number n_0 of defectives. The lot will be rejected if the portion of defectives is greater than this value. In this case the hypothesis that we are testing is that $p \leq p'$. Given the value of n_0 , if the first n_0 units inspected will be non-defective, the lot will be accepted. If in the first $m \leq n_0$ there is a unit that is defective, the lot will be rejected. The critical region is the key aspect of a sequential test. The principles of a proper choice of the critical region are based on the study of the consequences of any decision.

The critical region has been defined in the previous sections in the case the tolerable level of wrong

decision is known or based on cost-benefit considerations. Given the critical region we might want to investigate the degree of acceptance and rejection of the null hypothesis.

In the case there is only one unknown parameter ϕ in the process (i.e. the value of the predictor) the null hypothesis consists in $\phi \leq \phi_0$. The hypothesis will be accepted if the parameter is less or equal than the critical one and rejected if is greater. Lets now analyse the degree for acceptance and rejection. For example the rejection of the hypothesis is not considered a serious error if $\phi \leq \phi_0$ but near the boundary. Similarly the acceptance of the hypothesis will not be a serious error if the parameter is greater than the critical value but near the boundary of the critical area. If the point is right on the boundary the hypothesis may be accepted or rejected. The parameter space may be subdivided in three areas, the first one in which the acceptance is strongly preferred, the second one in which the rejection is strongly preferred and the last one in which there is no preference of acceptance or rejection. The subdivision of the space in the three areas gives an idea of the degree of preference for acceptance or rejection that will be better described by two functions of the parameter ϕ : f_0 that expresses the importance of the consequence of accepting the hypothesis when we should have not and f_1 the importance of rejecting the hypothesis when we should have not. For example in the zone of preference for rejection f_0 has a high positive value that represents the cost of acceptance, in this situation the f_1 will have a loss that will be very low. The dependence of preference for one action or another is related to the subdivision of the area of the samples in three areas, quantified by the functions f_0 and f_1 .

The functions f_0 and f_1 represent a guideline for decision making representing the degree of preference of one action or the other. The process consists not only in observing the parameter of interest but monitoring the functions f_0 and f_1 . These functions represent the consequences of taking action, i.e. false and missed alarm, loss caused by making a wrong decisions, etc.

In the following sections the decision process will be explained, based on sequential testing, during a seismic event, by monitoring the predictor and the functions representing the consequences of taking action.

The analysis has been first approached by choosing the probability of false and missed alarm as coincident to the f_0 and f_1 and then the analysis has been extended to the observation of other consequences as economic loss, structural damage etc (Chapter 8).

7.2. Operational aspects of EWS

During a seismic event, the probability of false and missed alarms will be updated with time as more stations are triggered by the seismic waves and more data comes in from those that have already been triggered. This increase in data available will produce a decrease with time in the

uncertainty in the predicted earthquake location and magnitude. Therefore, the prediction of the intensity measure can be updated with time and the characterization of its uncertainty, $\varepsilon_{\text{tot}}(t)$, will vary with time. As a consequence, it is important to update the probability of false and missed alarms as the seismic event evolves.

The necessity of a time-dependent method for the evaluation of the probability of false becomes essential. As more stations are triggered, the predictions (magnitude and epicentral distance) will be updated and their uncertainty as well, as a consequence the prediction of the intensity measure will be updated with time and its uncertainty, $\varepsilon_{\text{tot}}(t)$, function of time.

The IM that will be observed is unknown, the higher is the quality of the prediction the closer the value of the observed intensity measure will be to the prediction, that is a known parameter at each instant of time, when the predictions of magnitude and location and their uncertainties are available.

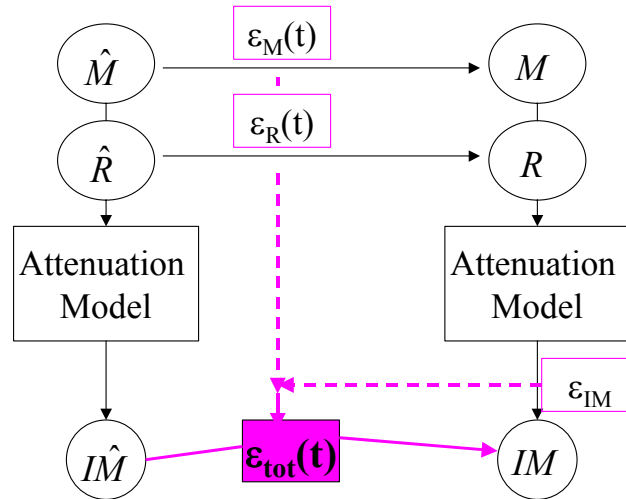


Figure 7.1 Simulation of the EWS prediction process, during the seismic event.

In a real-time analysis, during the seismic event, the information that results known is the prediction provided by the EWS prediction process, while in a off-line analysis the known parameter is the observation.

Given the prediction the value of the predictor that will be observed will be a value close or not to the prediction depending on the accuracy of the prediction process, represented by total error defined by the error analysis in the previous chapters.

The IM that will be observed may be assumed as a random variable of Gaussian distribution with mean equal to the prediction \hat{IM} and pdf given by the Bayesian approach (Virtual Seismologist Method, Cua and Heaton 2004) or by uncertainty propagation of the error.

The more the prediction process is accurate the more the distribution is peaked around the prediction. The assumption of IM normally distributed around the prediction is confirmed by the error analysis for ElarmS performance assessment, where from the results of the error analysis the

total error resulted well modeled by a Gaussain distribution.

In the real-time analysis the values of predicted magnitude, epicentral distance, provided by the EWS, will be used to estimate the predicted intensity measure IM , by the means of the attenuation model.

$$IM(t) = \hat{IM}(t) + \varepsilon_{tot}(t) \quad 7.1$$

Fundamental informations to be provided are the uncertainties of the predictions of M , R , ε_M , ε_R that as more data become available will be updated with time and will be used to define the total error related to the prediction, $\varepsilon_{tot}(t)$, characterized by a Gaussian distribution with zero mean and standard deviation given by uncertainty analysis (Chapter 4).

The total error represents the quality of the information provided by the EWS and is a basic information for consequences evaluation, representing the main source of wrong decisions.

7.3. Probability of wrong decisions in a real-time analysis

In this section we examine the decision-rule criterion chosen for decision making during the seismic event, that will represent the guideline to decide between raising the alarm and doing nothing.

The decision between an action or the other will be guided by the observation of the predictor and the degree of preference between the options.

The degree of preference may be considered as a measurable parameter. Degree of preference is considered to be connected to the concept of utility (Von Neumann and Morgenstern, 1945).

A numerical approach to utility is dependent on the possibility of comparing differences in utility. As an example for giving the sense of the measurable characteristic of utility as degree of preference of an event may be given by the very natural attitude of individuals to have a clear intuition of preferences of two objects or events. For any two alternatives the individual will associate probabilities. Associating a probability to an event or a combination of events he will intuitively prefer the one to the other. At same way the use of probabilities of errors will guide the user and define a rule for quantifying the preference for the possible actions, in our case raising the alarm or doing nothing.

A decision rule may be based on the probability of error criterion (Melsa and Cohn, 1978) related to the analysis of the probabilities of error. In our case the possible errors of interest are, as defined before, false and missed alarm. The total probability of error is defined as:

$$P_e = P_{el} + P_{ell} \quad 7.2$$

being the two conditions mutually exclusive.

The probabilities P_{el} and P_{ell} represent respectively the probability of a missed and of a false alert.

During the seismic event P_{el} and P_{ell} represent potential probabilities of wrong decision that will become probabilities of wrong decision when a decision is made.

In particular, the (potential) probability of false alarm is estimated as the probability of IM being less than the critical threshold, a , (if the alarm is raised becomes an probability of false alarm):

$$P_{fa}(t) = P[IM \leq a | \hat{IM}] \quad 7.3$$

Considering that the IM has a normal distribution with mean equal to the predicted \hat{IM} (if there is a known bias in the prediction μ_{tot} it should be added to this mean) and standard deviation σ_{tot} evaluated as a function of the updated uncertainties (uncertainty propagation methods, Chapter 4):

$$P_{fa}(t) = \int_{-\infty}^a \frac{1}{\sigma_{tot}(t)\sqrt{2\pi}} \exp\left[-\frac{(IM - \hat{IM}(t))^2}{2\sigma_{tot}(t)^2}\right] dIM = \Phi\left(\frac{a - \hat{IM}(t)}{\sigma_{tot}(t)}\right) \quad 7.4$$

where Φ is the standard Gaussian cumulative distribution function (Grasso et al., 2005 a).

The (potential) probability of missed alarm is equal to the probability of IM being greater than the critical threshold (if the alarm is not raised is the probability of missed alarm):

$$P_{ma}(t) = P[IM > a | \hat{IM}] \quad 7.5$$

$$P_{ma}(t) = \int_a^{\infty} \frac{1}{\sigma_{tot}(t)\sqrt{2\pi}} \exp\left[-\frac{(IM - \hat{IM}(t))^2}{2\sigma_{tot}(t)^2}\right] dIM = 1 - \Phi\left(\frac{a - \hat{IM}(t)}{\sigma_{tot}(t)}\right) \quad 7.6$$

Since the two conditions ($IM \leq a$ and $IM > a$) are mutually exclusive and exhaustive, the probabilities $P_{fa}(t)$ and $P_{ma}(t)$ always sum to one.

Probabilities of wrong decision are fundametal tools for decision making, representing our preference in one action instead of the other.

7.4. How EWS works during the event

In the operational situation the seismic EWS will provide information related to the estimates of

seismic parameters, magnitude and location of the event. Each end user of the EWS will receive in real-time these informations related to the incoming event.

How to use these informations? Before answering to this fundamental aspect, is important to point out the importance of sending informations on the quality of the predictions provided by the EWS.

The importance and the impact of uncertainty related to the predictor is fundamental at this point for decision making. Every end-user has to be provided not only by the estimates of the seismic parameters but also by the uncertainties related to it. The error probability distributions of magnitude and location will be provided by the EWS in the case of Bayesian update approach to the prediction process (as the Virtual Seismologist) or on the contrary in the case of traditional approaches to early warning it will be possible to use the results of the error analysis (as done for ElarmS in Chapter 4). In this case based on the statistical analysis based on off-line simulations associated to each instant of interest we will have error model of magnitude and of location.

At each second the EWS will provide the estimate of magnitude, location and related error models. At this point the estimates will be sent to user's central processing unit that will use the location of the event to estimate the epicentral distance. Magnitude and epicentral distance will be then used to evaluate the predictor of interest.

To the predictor has to be associated an uncertainty as well. The probability distribution function of the error of the predictor will be evaluated based on the considerations done for uncertainty propagation (Chapter 4). In the case the approximation method is applicable (for uncertainty propagation in Chapter 4), an estimate of ε_{tot} will be available in real-time. On the contrary a Monte Carlo simulation has to be done off-line and the results will be available in the real-time. For example a table has to be created, that associates the magnitude and the epicentral distance error models to the error model of the predictor of interest. In this way (approximation method or Monte-Carlo method) the error model of the predictor defining the quality of the information will be available in real-time. The estimate of the predictor and its uncertainty will be updated every instant of time. The availability of these informations, $\hat{IM}(t)$ and $\varepsilon_{tot}(t)$ enable the possibility of evaluating the consequences of taking action, representing our preference in an action or the other (alarm or doing nothing). Based on $\hat{IM}(t)$ and $\varepsilon_{tot}(t)$ a real-time estimate the potential probabilities of wrong decisions will be available (Eq. 7.4 and 7.6).

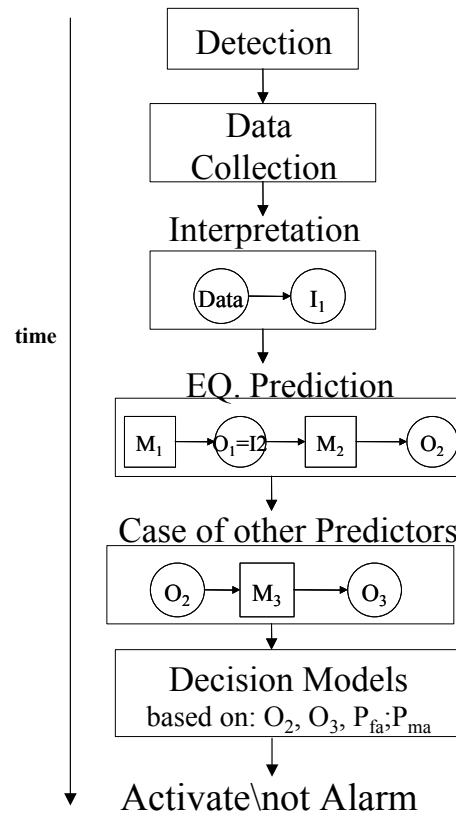


Figure 7.2 How EWS decision process works during a seismic event. The event is detected, the stations trigger the event and the registered data are collected and processed. The synthetic parameters are evaluated I_1 used to predict magnitude and location, O_1 (representing M and location) this information is then used to estimate the epicentral distance and the ground motion parameter (O_2). In the case of other predictors of interest the O_2 will be used to estimate O_3 (as engineering demand parameter etc.). In a parallel process the quality of the predictor is estimated and used to evaluate $P_{fa}(t)$ and $P_{ma}(t)$. The decision models based on this information will be a guideline for choosing to raise the alarm or do nothing.

7.5. Decision making during the event

Probabilities of wrong decisions represent a fundamental guideline for the user's decision making during the seismic event, that will represent a quantification of our belief in the information provided by the EWS.

In fact a decision based on pre-fixed threshold (adequate only for "special" cases as Mexico City and Bucharest, for which time-invariant approach is applicable) exceedance of the intensity measure predicted as a function of time during the event, could cause a false alarm, and the user will take a decision accepting a probability of wrong decision, without being aware of it.

A more rational decision can be based on real-time monitoring of the probability of wrong decisions, choosing the situation (false alarm or missed alarm) the user is more concerned about, that will be demonstrated that is equivalent to monitoring the predicted intensity measure exceedance of a time variant warning threshold, $c(t)a$.

The value of the probability (P_{fa} or P_{ma}) of interest, evaluated during the course of the event, is compared to the tolerable value (β or α), based on cost-benefit considerations (or provided by the user).

Monitoring the value of the probability of wrong decision of interest, during the event, the alarm will be raised when the value reaches the tolerable value.

This assumes that the time available is sufficient for activation of the protective measures. If the time available reaches the minimum time necessary for activation of the protective measure, the alarm will be raised only if the probability of a wrong decision, evaluated at that time, can be accepted.

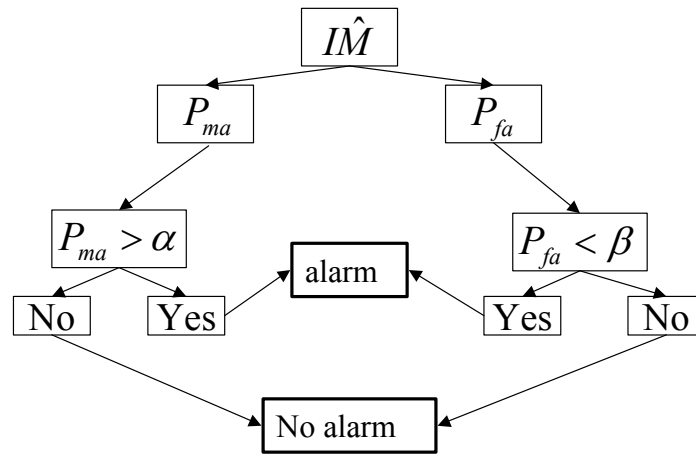


Figure 7.3 Decision making process based on probability of wrong decisions.

In the case the missed alarm is the situation of concern, in real-time the $P_{ma}(t)$ will be evaluated and compared to the tolerable level, from this condition the time-varying expression for the warning threshold can be derived:

$$\begin{aligned}
 P_{ma}(t) &= P[IM > a \mid \hat{IM}(t)] \\
 &= 1 - \Phi\left(\frac{a - \hat{IM}(t)}{\sigma_{tot}(t)}\right)
 \end{aligned} \tag{7.7}$$

$$P_{ma}(t) > \alpha \Leftrightarrow \hat{IM}(t) > a \left[1 - \frac{\sigma_{tot}(t) \Phi^{-1}(1 - \alpha)}{a} \right] = c_{ma}(t) \cdot a \tag{7.8}$$

Therefore, the setting of the alarm based on the probability of a missed alarm becoming unacceptable occurs if $\hat{IM}(t) > c_{ma}(t) \cdot a$ where:

$$c_{ma}(t) = 1 - \frac{\sigma_{tot}(t) \cdot \Phi^{-1}(1 - \alpha)}{a} \quad 7.9$$

The alarm is also set if the probability of a false alarm falls below the tolerable level β :

$$\begin{aligned} P_{fa}(t) &= P[IM \leq a \mid \hat{IM}(t)] \\ &= \Phi\left(\frac{a - \hat{IM}(t)}{\sigma_{tot}(t)}\right) \end{aligned} \quad 7.10$$

$$P_{fa}(t) < \beta \Leftrightarrow \hat{IM}(t) > a \left[1 - \frac{\sigma_{tot}(t) \Phi^{-1}(\beta)}{a} \right] = c_{fa}(t) \cdot a \quad 7.11$$

that is, the alarm is set if $\hat{IM}(t) > c_{fa}(t) \cdot a$ where:

$$c_{fa}(t) = 1 - \frac{\sigma_{tot}(t) \cdot \Phi^{-1}(\beta)}{a} \quad 7.12$$

If $\beta < 1 - \alpha$, then $c_{ma}(t) < c_{fa}(t)$ and so the concern about missing an alarm will control the setting of the alarm; on the other hand, if $\beta > 1 - \alpha$, then concern about causing a false alarm will control the setting of the alarm. Of course, making an alarm decision based on the exceedance of the predictor above the time-varying warning threshold is equivalent to monitoring the probability of $P_{fa}(t)$ and $P_{ma}(t)$ and raising the alarm based on exceedance of the tolerable level β and α , respectively.

It was pointed out in Chapter 6 that when the tolerable probabilities β and α to use during operation are based on cost-benefit considerations, they are related by: $\beta = 1 - \alpha$. Therefore, since the alarm probabilities and the tolerable probabilities sum up to one, the alarm probabilities will reach their critical thresholds at the same time, so one can choose to monitor either $P_{fa}(t)$ and $P_{ma}(t)$. Similarly, if the predictor $\hat{IM}(t)$ is monitored, the critical thresholds $c_{ma}(t)a$ and $c_{fa}(t)a$ are equal and so are reached at the same time (Grasso et al. 2005 a,b).

7.6. Decision making during a seismic event: simulation of the decision procedure during California Earthquakes

7.6.1. Yorba Linda M=4.75

The 3 September 2002, Yorba Linda earthquake occurred in California, in Orange County, with magnitude 4.75. The epicenter has been located at 33.9173° N and -117.7758° W with a depth of

12.92 Km. The main shock was anticipated by two foreshocks of magnitude 2.66 and 1.6, occurred 24 hours before the main shock.

The area of the main shock is densely instrumented and the first station triggering the event is the Serrano (SRN) station at 9.9 Km from the epicenter. The prediction of the seismic parameter during the evolution of the event used for the decision model simulation of the real-time analysis is carried out by the Virtual Seismologist method (Cua and Heaton 2004).

After the first 3-second after the P-wave detection the first estimate of magnitude and location is done by the Virtual Seismologist method. Due to the high density of stations in the epicentral area the location is uniquely determined. This is a special case and the most favorable for the method testing. Cua and Heaton (2004) have defined as a function of time the most likely estimates of magnitude and location at 5, 8, 13, 38, and 78 seconds after the initial P arrival.

The first station to be triggered SRN defines the Voronoi cell that constrains the location of the event. The event is located within the Voronoi cell. Using data only from the first station the method defines magnitude and epicentral distance or magnitude and location coordinates.

The discriminant function that is a function of maximum vertical acceleration, velocity and displacement and the corresponding envelope amplitudes for the root mean square of the maximum amplitudes of the horizontal channels. The discriminant function is evaluated in real-time and defines the P and S arrivals. The function is evaluated at station SRN, the zero crossing of the function, after P arrival, defines the S arrival. For values greater than zero it corresponds to P wave for values of the function less than zero value is related to S wave.

The accuracy is of 15%. The magnitude estimate is related to the evaluation of the ground motion ratio that is a function of the logarithm of the acceleration amplitude and the logarithm of the displacement amplitude (peak vertical ground motions). The values of the ratio are compared to decision boundaries in order to define the range of corresponding magnitude. The ground motion ratios estimated for SRN station indicate a magnitude between 5 and 6.

At this point the likelihood function $p(data | M, R)$ which combines the magnitude estimates from the vertical acceleration and displacement ground motion ratio, along with the peak available vertical velocity, and rms horizontal acceleration, velocity, and displacement amplitudes, is estimated.

Maximizing the likelihood function an estimate of magnitude and location will be obtained. The most probable values of M and R are included in the high probability area, unfortunately the trade-off between M and R cannot be solved using only the first 3 sec of data from only one station.

Considering the 3 sec of P wave coming from SRN station an estimated magnitude of 5.5 and

location of 33 Km from SRN station is estimated from the Virtual Seismologist method.

Different prior informations $p(M, R)$ can be considered in the process in order to solve the trade-off, as Gutenberg-Richter law for magnitude distribution, Voronoi cells to constrain the locations, and finally previously observed seismicity, so to take in account foreshocks occurred in the area of interest. The Voronoi cell of SRN may be used to construct the pdf of locations and the Gutenberg-Richter law defines the most probable magnitudes, smaller events are more probable than bigger magnitude events.

The most likely predictions of magnitude and location are those that maximize the posterior given by:

$$p(M, R | data) \propto p(data | M, R) \cdot p(M, R) \quad 7.13$$

where $p(data | M, R)$ represents the likelihood and $p(M, R)$ the prior.

Cua (2004) assumes that the prior is given by the product of the prior of magnitude and the prior of epicentral distance assuming magnitude and location information to be independent.

Considering the Gutenberg-Richter law and the first 3 sec of P wave from the first station, a magnitude of 4.4 and location of 8 Km from SRN is predicted.

Multiple station update is also considered for magnitude and location estimate. In this case is included prior seismicity considering foreshocks occurred 24 hours before the main shock and the station geometry prior related to the Voronoi cell of station SRN that first triggers the event. During the first 3 seconds already 7 stations are triggered. Again Gutenberg-Richter law is used to create the magnitude prior. The Bayesian prior is then evaluated as the product of the prior of magnitude and of location. The error of location is 0.89 Km and the magnitude, without including the Gutenberg-Richter prior, is 4.8.

Prior information becomes fundamental for solving the trade-off between magnitude and location but becomes unnecessary when there is enough data available to find a uniquely determined solution as in this case due to a high station density.

Gutenberg-Richter prior for magnitude and multiple station approach has been considered.

In this case the location error is within 4 Km of the reported epicenter and the error stabilizes at 4 seconds. While the magnitude estimate varies as described in the Fig. 7.4.

At this stage the epicentral distance prediction is considered time invariant, assuming, Kanamori personal communication, that the error associated with magnitude is more influent in the IM prediction process as confirmed in the error analysis for ElarmS sensitivity analysis (Chapter 4).

Magnitude uncertainty is assumed to decrease as $1/\sqrt{N}$ where N is the number of station contributing information to the Virtual Seismologist method (Fig. 7.5).

Based on these assumptions:

- ε_M : Gaussian $(0, \sigma_M)$ where $\sigma_M = 1/\sqrt{N}$
- ε_R : ignored at this stage
- ε_{IM} : Gaussian $(0, 0.243)$

The total error associated to the predicted \hat{IM} , is defined as in Chapter 4:

- ε_{tot} : Gaussian $(0, \sigma_{tot})$

In the Virtual Seismologist method the amplitude is defined as:

$$\log(A) = aM - b \times (R_l + C(M)) + -d \log(R_l + C(M)) + e + \varepsilon \quad 7.14$$

where M is the magnitude; R_l depends on R which is the epicentral distance; $C(M)$ is a correction factor depending on magnitude. The residual term ε is a zero mean error term representing the prediction uncertainty (the so called ε_{IM}) and e is a constant error which includes station corrections; the parameters a, b, d, e are defined by the model's calibration by data fitting, in this case rock soil has been considered.

The epicentral distance is assumed to be 10 Km.

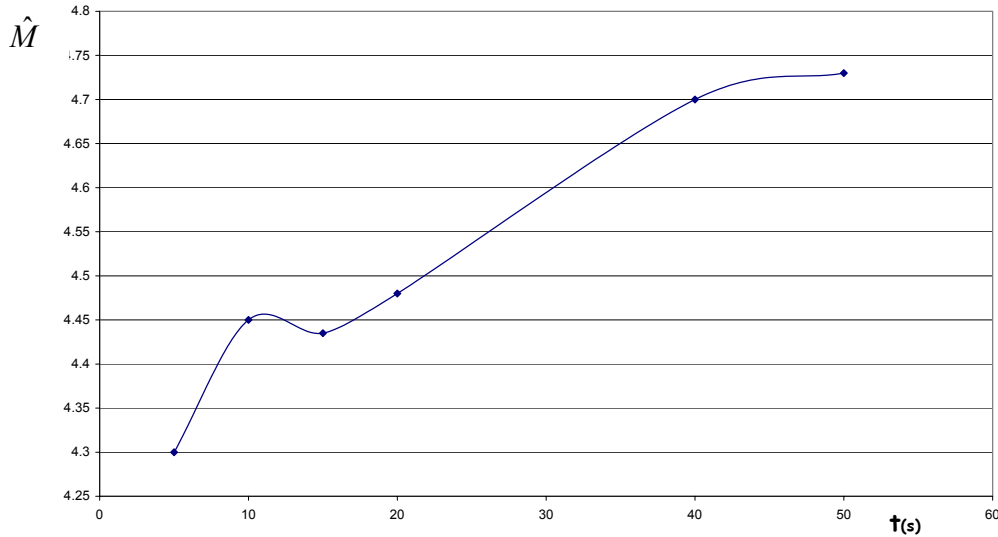


Figure 7.4 Yorba Linda M=4.75. The Virtual Seismologist Magnitude estimate as a function of time evaluated by Bayesian update considering multiple station data and Gutenberg-Richter magnitude prior. Note that the observed magnitude is equal to 4.75. Magnitude is underestimated due to the influence of the Gutenberg-Richter prior that tells that smaller events are more probable than bigger ones.

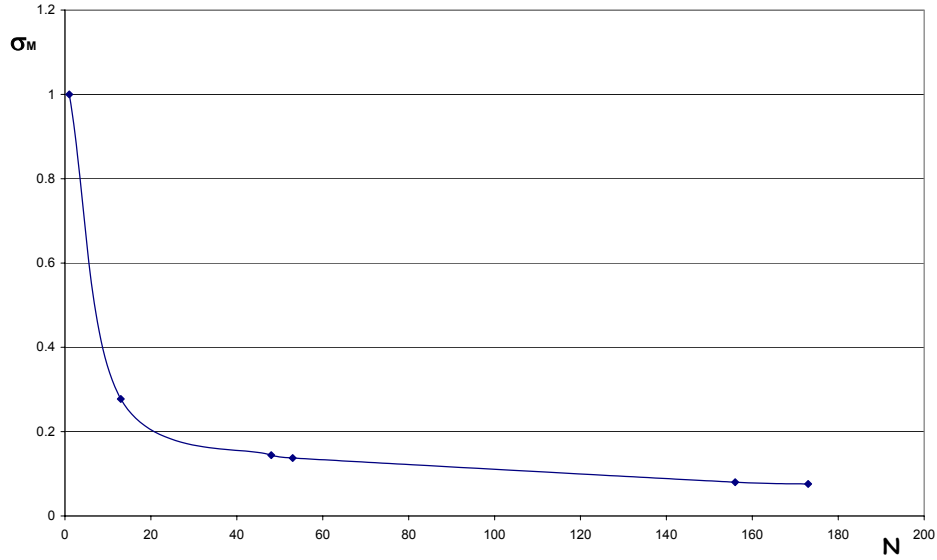


Figure 7.5 Yorba Linda M=4.75. Magnitude uncertainty as a function of the number of stations contributing observations to the Virtual Seismologist estimate.

At each prediction update the probabilities of wrong decisions are evaluated, as a fundamental tool for decision making.

In Fig. 7.6 are represented, as a function of time, the intensity measure prediction, the standard deviation of the prediction error and, the probabilities of wrong decisions are evaluated, assuming the critical threshold $\alpha=1.4$ (in \log_{10} scale in cm/s/s) following Eq. 7.4 and 7.6.

The probabilities of wrong decisions are used to make a decision during the event, raise the alarm or not, based on threshold exceedance of the tolerable values of P_{fa} or P_{ma} , evaluated based on cost-benefit considerations.

As demonstrated before decision making approach is equivalent the case of monitoring \hat{IM} , P_{fa} or P_{ma} so in this case P_{fa} is chosen.

In Fig. 7.7 is represented the P_{fa} as a function of time and when the tolerable value (β is 0.4) is reached the alarm is raised, if the minimum warning time for security measure activation is not reached before. Note that when P_{fa} reaches β , the predictor \hat{IM} reaches the warning threshold, $c(t)a$, demonstrating that a decision can be made either monitoring P_{fa} (or P_{ma}) either the predictor, \hat{IM} . If the warning time reaches the minimum time necessary for security measure activation before P_{fa} reaches the tolerable level a decision has to be made. Based on the value assumed by P_{fa} at the time of minimum time required for alarm activation the alarm will be raised if this value is acceptable.

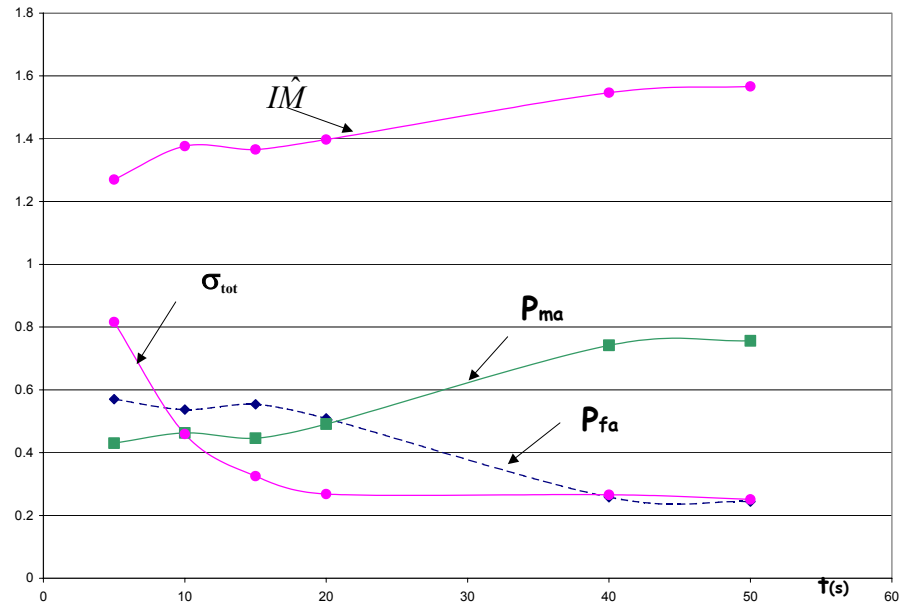


Figure 7.6 Yorba Linda 2002: Evolution of the prediction of IM, the standard deviation of magnitude prediction and the probabilities of wrong decisions (false and missed alarms) with time.

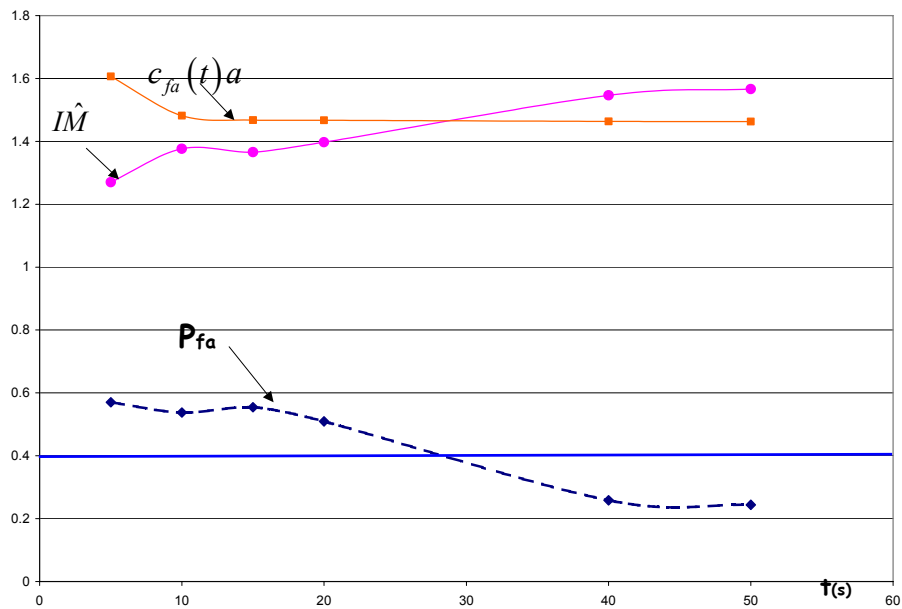


Figure 7.7 Yorba Linda M=4.75. Decision making based on cost-benefit considerations.

7.6.2. San Simeon M=6.5

22 of December 2003 San Simeon earthquake occurred in central coast of California, with magnitude 6.5.

The mainshock has been located in 35.702° N and 121.08° W with a depth of 7 Km causing two casualties in the town of Paso Robles.

The closest station to the epicenter is Parkfield that first triggered the event, located at a distance of 57 Km (Cua 2004).

Unfortunately the area is not densely instrumented, the data available were not as many as for Yorba Linda event, described before. The event occurred at the boundary between the Southern California Seismic Network and the Berkeley Digital Seismic Network.

In this case the San Simeon event is interesting to test the Virtual Seismologist method and the decision models for larger events at the boundary of the network.

From Virtual Seismologist method (Cua and Heaton 2004) the predictions for magnitude and location are available at 3, 5.5, 8, 31 and 71 seconds after the first station triggered the event.

The Virtual Seismologist method for estimates updating considers the previous seismicity, Gutenberg-Richter law, the San Andreas fault as the Bayes prior for magnitude and location. Two earthquakes occurred in the 24 hours before the mainshock that have been located at the San Andreas fault and at 8.5 Km from the epicenter, respectively.

The first triggering station, Parkfield station, defines the Voronoi cell that constraints the epicenter location. The cell defines the area of the most likely locations that occurs to be fairly sparse due to the low density of the stations in the area.

The second station, Park Hill, is triggered almost at the same time of the first one. As a consequence the Voronoi cell defining the possible locations shares an edge with the Voronoi cell of Parkfield station. Looking at the first 3 seconds of P waves considering only the first triggered station, the Virtual Seismologist method cannot solve the trade-off between magnitude and location due to inadequate volume of data. Although maximizing the likelihood function a value of 6.7 of magnitude and a location at 158 Km away from Parkfield, is estimated (San Simeon had $M=6.5$ located 57 Km away from Parkfield).

Taking into account further station's information helps to solve the trade-off and obtain more accurate estimates.

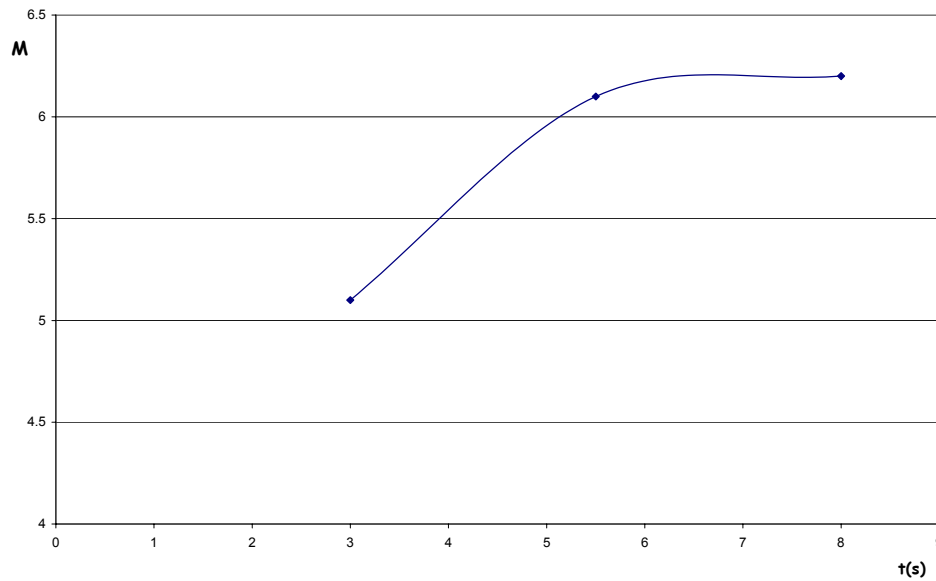


Figure 7.8 San Simeon $M=6.5$. The Virtual Seismologist Magnitude estimate as a function of time evaluated by Bayesian update considering multiple station data and Gutenberg-Richter magnitude prior. Note that the observed magnitude is equal to 6.5. Magnitude is underestimated due to the influence of the Gutenberg-Richter prior that tells that smaller events are more probable than bigger ones.

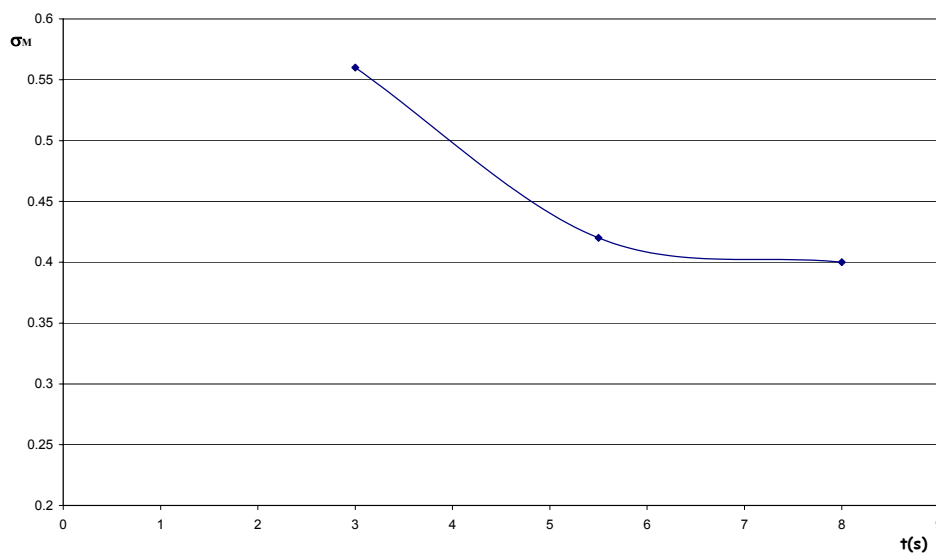


Figure 7.9 San Simeon $M=6.5$. Magnitude uncertainty as a function of the number of stations contributing observations to the Virtual Seismologist estimate.

The magnitude estimate varies as in the Fig. 7.8.

At this stage the epicentral distance prediction is considered time invariant, assuming, Kanamori personal communication, that the error associated with magnitude is more influent in the IM prediction process as confirmed in the error analysis for ElarmS sensitivity analysis. The epicentral

distance is assumed to be equal to 57 Km.

Magnitude uncertainty is assumed to decrease as $1/\sqrt{N}$ where N is the number of station contributing information to the Virtual Seismologist method (Fig. 7.9).

Based on these assumptions:

- ε_M : Gaussian $(0, \sigma_M)$ where $\sigma_M = 1/\sqrt{N}$
- ε_R : ignored at this stage
- ε_{IM} : Gaussian $(0, 0.243)$

The total error associated to the predicted \hat{IM} , is defined as in Chapter 4:

- ε_{tot} : Gaussian $(0, \sigma_{tot})$

In the Virtual Seismologist method the amplitude is defined as from Eq. 7.14. The ground motion parameter estimate (PGA in \log_{10} scale in cm/s^2) is described in Fig. 7.10.

At each instant of time, as the estimates of magnitude and location are updated by the Virtual Seismologist, the ground motion parameter is updated.

The probabilities of wrong decisions are evaluated (based on Eq. 7.4 and 7.6) and used as a tool for decision making during the event, assuming $\alpha=1.4$ (in \log_{10} scale in cm/s^2) (Fig. 7.10-7.11).

The probabilities of wrong decisions are used in the decision model in order to make a decision during the event, raise the alarm or do nothing, based on threshold exceedance of the tolerable values of P_{fa} or P_{ma} , evaluated from a cost-benefit analysis.

As demonstrated before is equivalent the case of monitoring \hat{IM} , P_{fa} or P_{ma} so in this case P_{fa} is chosen for making the decision of raising the alarm or doing nothing.

In Fig. 7.11 is represented the P_{fa} as a function of time and when the tolerable value is reached the alarm is raised, if the minimum warning time for security measure activation is not reached before.

If the warning time reaches the minimum time necessary for security measure activation before P_{fa} reaches the tolerable level a decision has to be made. Based on the value assumed by P_{fa} at the time of minimum time required for alarm activation the alarm will be raised if this value is included in a tolerance zone.

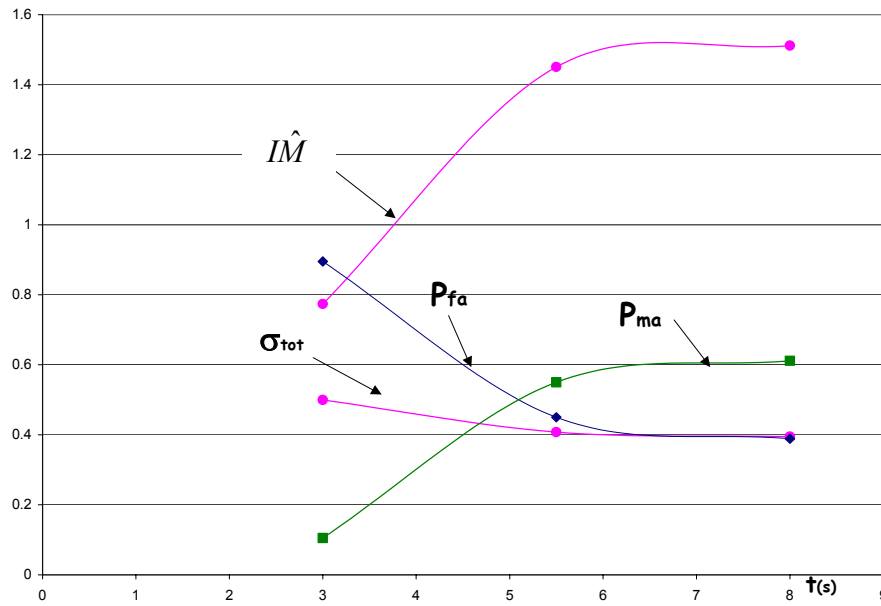


Figure 7.10 San Simeon M=6.5. Evolution of the prediction of IM , of the standard deviation of prediction error, of probabilities of wrong decions (false and missed alarm) as a function of time.

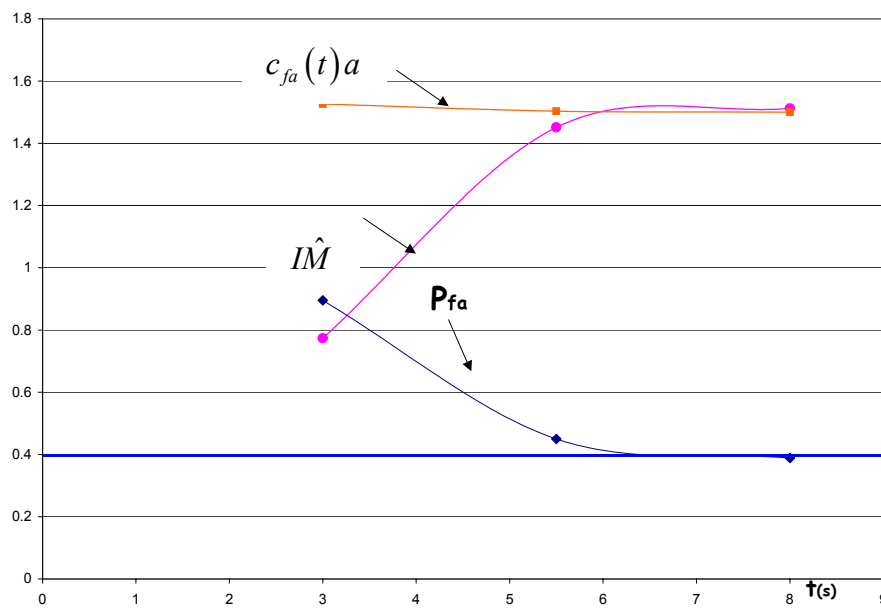


Figure 7.11 San Simeon M=6.5. Decision making based on cost-benefits considerations.

7.7. Extension to other predictors than IM

Decision making could be based on other decision variables than probability of wrong decisions, that represent the expected consequences in terms of structural behaviour, damage or economic

losses.

The theory that has been laid out in the previous paragraphs could be readily extended to other predictors of interest by the PBEE framework (Chapter 8), as engineering demand parameters, as drift, spectral acceleration, expected damage or losses, in terms of loss of lives or economic losses, due to the incoming seismic event (Grasso et al., 2005 a,b).

The real-time analysis will be based on monitoring probabilities based on engineering parameters of interest or expected consequences, instead of the intensity measure.

The analysis will be an extension of the previous expressions, using the theory of the total probability, e.g. extending the probability of missed alarm based on IM to an engineering demand parameter (EDP):

$$\begin{aligned} P_{ma}(t) &= P[EDP > e | \hat{IM}] \\ &= \int_0^{\infty} p(EDP > e | IM) p(IM | \hat{IM}) dIM \end{aligned} \quad 7.15$$

Where e is the threshold value of the EDP .

The probability can be extended to the estimate of the probability of damage or loss:

$$\begin{aligned} P_{ma}(t) &= P[DV > d | \hat{IM}] \\ &= \int_0^{\infty} p(DV > d | EDP) p(EDP | IM) p(IM | \hat{IM}) dIM \end{aligned} \quad 7.16$$

Where DM is the decision variable, e.g. expected damage or loss, and d is the threshold.

Chapter 8

8. Performance-Based Earthquake Early Warning-PBEEW

8.1. PBEEW for performance assessment and design: Background

PBEEW may be interpreted as an extension of Performance-based earthquake engineering (PBEE) method for the quantification of structural performance, fatalities, repair costs, and repair duration of a building subject to a seismic event.

Before introducing PBEEW is fundamental to describe PBEE methodology. In the PBEE framework as in Fig. 8.1 (Beck et al. 1999, 2002) more level of seismicity are considered, the expected structural analysis is performed via dynamic analysis, the damage is calculated based on the structural performance, finally damage is used to evaluate loss (Beck et al. 2004).

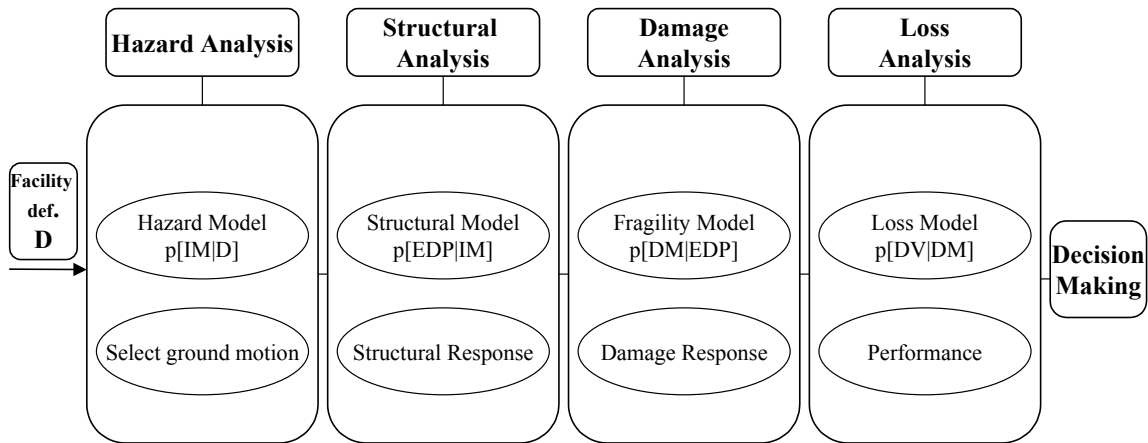


Figure 8.1 PBEE frame-work (Porter et al. 2004).

From a structural design perspective PBEE represents an innovative design approach opposed to load-and-resistance-factor design (LRFD). The goal of LRFD is to assure the performance in terms of failure probability of single components, on the contrary PBEE looks at the performance at a system level, in terms of risk of collapse, repair cost, downtime (Porter, 2003).

PBEE works in four stages: hazard analysis, structural analysis, damage analysis and loss analysis. Hazard analysis consists in defining the seismic hazard at the facility site characterized by Hazard function.

In Hazard analysis sample time-histories are chosen as representative of various levels of intensity IM for various hazard levels (i.e. 10%, 5%, and 2% exceedance probability in 50 years). Procedures for time-history selection is described in Somerville and Collins (2002).

Structural analysis is pursued to calculate the structural response correspondent to various intensity

measures of the ground motion. Various non-linear structural analysis are carried out in order to evaluate structural response in terms of drifts, accelerations, or other *EDP*. The uncertain structural response is defined by the probability distribution function of *EDP* conditioned to seismic excitation, *IM*. PEER analysis includes mass, damping, and force-deformation uncertainty treatment.

In damage analysis the *EDPs* are used to evaluate the parameter state of damage *DM* by the means of fragility functions of the single components. The decision variable *DV*, that may be repair costs, operability and others, is evaluated based on *DM*. The probability of various damage levels *DM* is conditioned on structural *EDP*. The final stage is represented by the evaluation of the performance expressed in terms of probability of various levels of *DV* conditioned on damage *DM*.

The output of the method is the performance in terms of probabilistic estimates of repair costs, casualties, loss. For a given facility at a given location the performance may be evaluated for a certain period of interest as the probability of exceeding various levels of interest, of a certain decision variable of interest. Frequency and probability distribution functions of a decision variable of interest are evaluated to be used eventually to evaluate single values (i.e. the expected value) of interest for facility stakeholders.

PBEE method is a probabilistic approach for performance estimation taking into account uncertainty associated with each of the four phases of the process. In the Hazard analysis is considered as uncertain the level of intensity measure of the earthquake that will occur. The structural model is uncertain itself, its mass, damping and force-deformation behaviour. Damage and loss analysis are affected by uncertainties as well.

The impact of each source of uncertainty has been estimated for the Van-Nuys PEER testbed. The test-bed consists in applying PEER methodology to a specific facility, in this case Van-Nuys hotel located in San Fernando valley in California. A simple deterministic study (Porter, 2003) has been conducted evaluating the change in output considering uncertain input once at the lower bound and once at the upper bound. The uncertain parameters which has the most significant impact on the uncertainty of the expected loss are the component fragility, maximum spectral acceleration that the facility will experience and ground motion details. Uncertain unit repair cost, force-deformation behaviour, damping do not contribute significantly on loss uncertainty.

8.2. PBEEW for performance assessment and design

Performance based earthquake early warning is a method for performance assessment at the system level in terms of collapse, fatalities, repair cost and post-earthquake loss. The system in analysis is composed by the EWS and the control system that provides the activation of security measures, in

case of the decision variable of interest exceeds the threshold for a given facility and given location. The output of the procedure is a probabilistic representation of the system's performance, expected under the uncertain ground motion that the facility will experience.

Opposed to PBEE method the system in PBEEW is represented by the target facility and the EWS. PBEEW is a probabilistic method that takes into account the uncertainty associated with Hazard analysis, structural analysis, damage analysis and loss analysis, in addition uncertainty associated to EWS prediction is considered. The system performance is affected by the uncertainty of EWS prediction. The prediction error is propagated through the output for performance evaluation. From Hazard analysis sample time-hystories are chosen characterized by various levels of IM , then to take into account the EWS uncertainty, the value of IM is affected by a prediction error. Assuming a Gaussian distribution for the prediction error, the distribution of the prediction will be characterized by a mean of $IM \pm \mu_{tot}$ and standard deviation of σ_{tot} given by error analysis (Chapter 4). For a certain IM level, lets indicate it as IM' , several values of IM will be chosen from the distribution characterized by a mean of $IM' \pm \mu_{tot}$ and standard deviation of σ_{tot} , for each value the structural performance will be estimated. Structural analysis are performed in order to estimate the structural behaviour in terms of EDP . Structural performance will be evaluated as the probability of EDP conditioned on IM . Damage analysis estimates the probability distribution of DM conditioned on EDP . Finally system performance is estimated by evaluating the probability distribution of DV conditioned on DM . PBEEW differs from PBEE in taking into account the EWS prediction uncertainty, obtaining the system performance, considering theorem of total probability:

$$p(DV) = p(DV | DM) p(DM | EDP) p(EDP | \hat{IM}) p(\hat{IM} | IM) p(IM) \quad 8.1$$

where $p(IM)$ may be derived from the Hazard function as in section 5.2 and $p(\hat{IM} | IM)$ is a Gaussian distribution with mean $IM \pm \mu_{tot}$ and standard deviation σ_{tot} given by error analysis, Chapter 4.

From Eq. 8.1 useful information for facility stakeholders may be derived, as probability of exceedance of a threshold level of concern, d :

$$P[DV > d] = \int \int \int P(DV > d | DM) p(DM | EDP) p(EDP | \hat{IM}) p(\hat{IM} | IM) p(IM) dIM dEDP dDM \quad 8.2$$

8.3. PBEEW for Real-Time Loss estimation: Background

Based on PBEE methods, availability in real-time of seismic data, advances in structural identification and damage detection, Porter et al. 2004 propose a method for (near) real-time loss estimation for instrumented buildings after the cessation of ground shaking. The goal of the method

is the development of a near-real-time method for the evaluation of probabilistic damage, repair cost, safety and operability for an instrumented building where have been located accelerometers at the base, any additional instrumentation are used to reduce structural model uncertainty. The advantage of the method is represented by availability of safety and operability information for emergency management, safety assessment and prioritizing operations for safety inspections, damage assessment reduces costs of business interruption and building evacuation, funding procedures may be simplified and speed up.

8.3.1. An overview

An instrumented facility is considered by Porter et al. 2004, defined by structural and architectural design. The structural model, accounting the uncertainty of the structural parameters, is a stochastic model defined by probability distributions to describe the uncertain structural parameters.

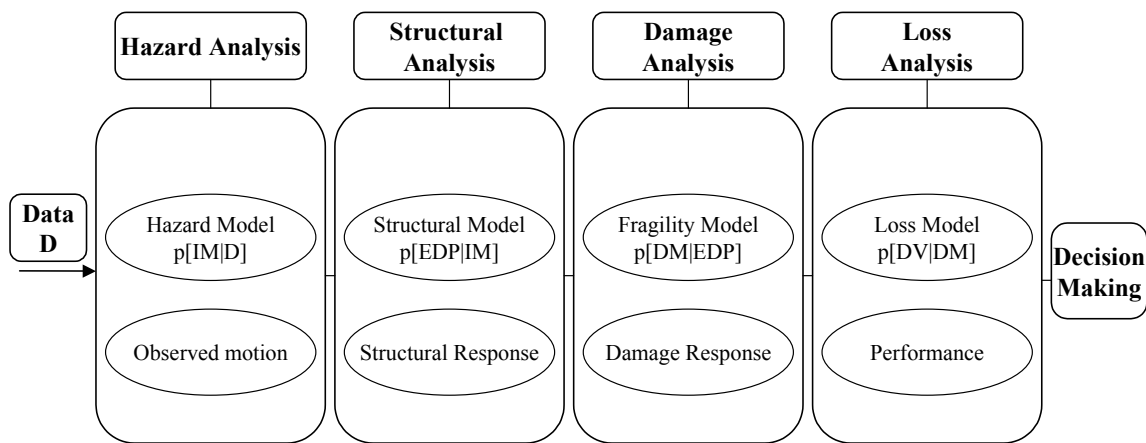


Figure 8.2 Near-real-time loss estimation based on PBEE frame-work (Porter et al. 2004).

Different structural parameters are treated as uncertain: damping, initial and post-yield stiffness, and structural strength. Randomly sampling from these distributions, N realizations of the structural model are created. When an earthquake occurs, the accelerations are registered by the sensors at different locations of the structure. The real-time registrations are used for performing structural analysis. For each structural realization a non-linear time-history structural analysis is performed. From each structural analysis the sample engineering demand parameter (EDP) is evaluated. A bayesian updating process is used to evaluate weighting factor w_i , by comparing calculated and observed accelerations, to apply to each simulation, details may be found in Porter et al. 2004. Each sample EDP is used to define physical damage of each damageable assembly. A vector of N damage measures DM is obtained. Then for each DM the decision variable DV (i.e. repair cost, life-safety, etc.) is estimated based on the loss model. The output of the analysis is a vector of N

elements (w_i, DV_i) that is used to build the probability distribution of a DV :

$$F_{DV}(dv) = P[DV \leq dv] = \sum_{i=0}^{N-1} w_i H(dv - DV_i) \quad 8.3$$

where $H(x)=1$ if $x \geq 0$ and $H(x)=0$ in the other case, H is the Heaviside function (Porter et al., 2004).

8.4. PBEEW for Real-Time Loss estimation

Performance based earthquake early warning (PBEEW) is a proposed methodology based on PBEE. In particular PBEEW is an extension of PBEE to early warning. PBEEW goal is to enable the possibility of providing performance assessment, expected loss, expected operability, and safety before the strong shaking occurs at the “target” location, representing an important decision variables for decision making.

The interest in PBEEW raises related to the possibility of performing automated loss analysis that provides expected loss estimates before the strong shaking occurs at the “target” facility. In early time information on repair cost, losses, safety and operability will be available. Expected physical damage of the structure will be available, useful data for effective emergency management strategies. The proposed PBEEW method is based on Porter et al. (2004) near-real-time loss estimation for instrumented buildings. In particular in PBEEW is proposed as an interaction between PBEE and EWS.

Another interesting option for real-time loss analysis may be the possibility of interfacing maps of shaking intensity, Shake Map, produced by TriNet, available in real-time by an EWS, with HAZUS (FEMA,1999) providing loss maps (Porter et al., 2004). Although HAZUS provides loss maps that may be considered reliable for a large scale assessment while in small scale HAZUS loss map is only approximate. On the contrary PBEEW real-time performance estimate is more accurate.

For PBEEW the fundamental data are represented by the characteristics required to describe the “target” structure for loss estimation (as in Porter et al. 2004) represented by location, structural and architectural drawings, geotechnical reports and occupancy during the daytime and night. These information are useful to define the damageable assemblies and to model the structure for non-linear time-history structural analysis. In PBEEW case an instrumented building is not necessary, the information on EDP comes from EW early estimates. The EWS provides in real-time location and magnitude estimates and based on these values an IM prediction is based. Based on IM a prediction of EDP may be available based on structural response from off-line non linear structural analysis.

The frame-work of PBEEW is represented in the following figure.

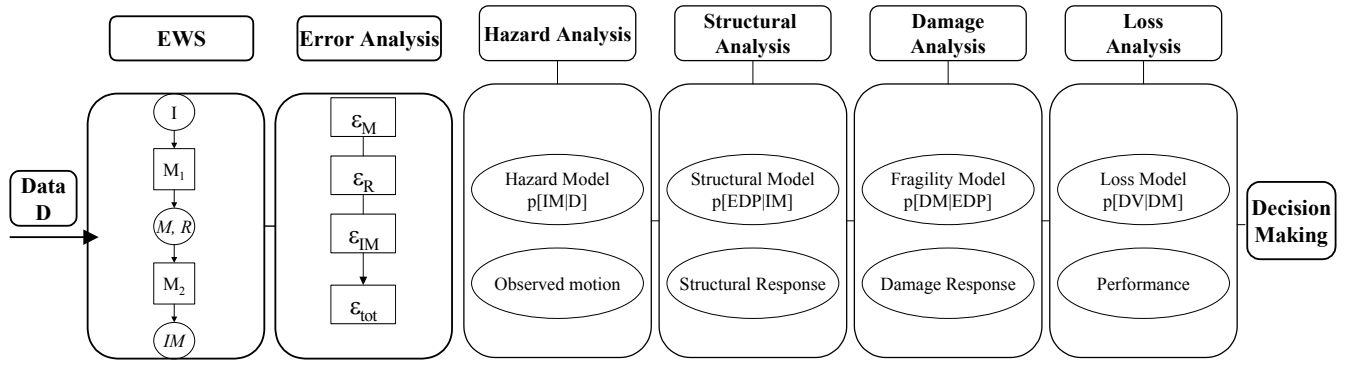


Figure 8.3 PBEEW frame-work

The data D coming from the seismic network are registered by the stations and processed in real-time. The data D are processed by the central processing unit (or by the single nodes) by the use of prediction models M_1 and M_2 represented under the EWS tag. The prediction process has been described in chapter 4. The output of the EWS is the prediction of the ground shaking intensity expected at the “target” site facility. Error analysis is necessary to evaluate the uncertainty associated with the prediction by the means of the approximation method or Monte Carlo method described in Chapter 4. The expected intensity measure, IM , and its uncertainty are then used to estimate $p(IM | \hat{IM})$ equivalent to $p(IM | D)$ that has a Gaussian distribution with mean equal to $\hat{IM} \pm \mu_{tot}(t)$ and standard deviation $\sigma_{tot}(t)$ from uncertainty analysis (section 2.3). The mean and standard deviation of the distribution $p(IM | \hat{IM})$ are updated with time, as more data become available. The structural response for time saving may be evaluated on the basis of off-line structural analysis that provides $p(EDP | IM)$. A large number of structural realizations may be created to consider the structural parameter uncertainties and for each model a non-linear structural analysis is performed. The goal is to obtain the relation between the IM and the EDP of interest. A functional relationship may be found between the IM and the EDP of interest and the uncertainty to it associated (as in Barroso and Winterstein (2002) where a power relationship is suggested considering the spectral acceleration as IM and drift as EDP of interest).

Damage response is estimated on the basis of damage model. In the damage analysis the damage is evaluated for each damageable assembly based on fragility functions. Fragility function provides the probability that the assembly would reach or exceed a damage state when subject to a certain EDP . Porter et al. 2004 suggest to consider the fragility functions as cumulative lognormal distribution functions, where if x_m is the median value of the distribution and β_s the standard deviation:

$$F_{R, dm}(x) = \Phi\left(\frac{\ln(x/x_m)}{\beta_s}\right) \quad 8.4$$

where Rdm is the threshold level EDP to cause a damage level dm of the assembly. For each assembly and dm associated we have a mean x_m and standard deviation β_s to define the fragility curve determined by testing or analytical evaluation (Porter et al 2004).

At this point is necessary to calculate the probability distribution function of DM conditioned to EDP that is given by the cumulative distribution function:

$$\begin{aligned} F_{DM|EDP}(dm) &= P[DM \leq dm | EDP = x] \\ &= 1 - F_{Rdm+1}(x) \end{aligned} \quad 8.5$$

based on DM the decision variable DV has to be evaluated.

The interest is focused on repair cost as decision variable of interest. Repair cost is evaluated by cost-estimation analysis.

The uncertain cost C_{jdm} to restore an assembly from damage level dm is defined by a cumulative distribution function as suggested by Porter et al (2004) F_{Cjdm} lognormally distributed characterized by mean x_m and logarithmic standard deviation β_s specified for each assembly type and damage state. The cost of the contractor C_c is considered to be 15% or 20% of the total cost.

The repair cost is defined by (Porter et al 2004):

$$RC = (1 + C_c) \sum_{j=1}^{N_j} \sum_{dm=1}^{N_{DM}} N_{j, dm} C_{j, dm} \quad 8.6$$

where j is the type of assembly, $N_{j, dm}$ is the number of damaged assemblies in damage level dm .

The cumulative distribution function of the decision variable is calculated by (Porter et al 2004):

$$F_{DV}(dv) = P[DV \leq dv] = \sum_{i=0}^N w_i H(dv - RC_i) \quad 8.7$$

where H is the Heaviside function and w_i is the weight assigned to each simulation (Porter et al. 2004 for the details).

The final output of the method is a probability distribution of a DV , in this case the repair cost is the decision variable of interest:

$$p(DV) = p(DV | DM) p(DM | EDP) p(EDP | IM) p(IM | \hat{IM}(t)) \quad 8.8$$

where $p(IM | \hat{IM})$ comes from \hat{IM} based on EW estimates and error analysis, is a Gaussian distribution with mean $\hat{IM} \pm \mu_{tot}$ and standard deviation $\sigma_{\epsilon_{tot}}$ given by error analysis, Chapter 4; $p(EDP | IM)$ is the output of structural analysis, $p(DM | EDP)$ comes from damage analysis and finally $p(DV | DM)$ (Eq. 8.7) is the outcome of loss analysis, in the case of repair cost as decision variable of interest.

From Eq. 8.8 an important information may be estrapolated, as the probability of exceedance of a decision threshold:

$$P[DV > d | \hat{IM}(t)] = \int \int \int P(DV > d | DM) p(DM | EDP) p(EDP | IM) p(IM | \hat{IM}(t)) dIM dEDP dDM \quad 8.9$$

Chapter 9

9. Conclusions and Future Directions

From a review of existing EWS applications in Japan, Mexico, Taiwan and Turkey (Espinosa Aranda *et al.*, 1995; Wu *et al.*, 1998; Wu and Teng, 2002, Erdik *et al.*, 2003; Boese *et al.*, 2004; Horiuchi *et al.*, 2005) emerges a mandatory need of approaching EWS from user's perspectives, both in analysis and design.

In this sense theory of ergonomics comes of some help for system optimization based on user's requirements.

This thesis presents the development of a performance-based methodology for EWS analysis and design.

The methodology seeks to provide a probabilistic description of the system performance (in terms of probability of making wrong decisions, expected losses, damage, etc.) in a pre-installation scenario for feasibility assessment of new and existing EWS applications. An example is shown for Southern California .

In addition is also explored the real-time case, the methodology presented in Chapter 7-8 develops a decision making strategy for deciding whether raising the alarm or not, based on EWS performance evaluated during the course of the seismic event (in terms of probability of making wrong decisions, expected losses, damage, etc.). The methodology has been applied to Yorba Linda and San Simeon seismic events.

Many theoretical and practical issues has to be solved. Which are the best indicators of EWS performance? What is required to demonstrate that EWS offers new value to owners and facility stakeholders? Which information decision makers would like to know in a pre-installation phase in order to evaluate the benefits of applying EWS for seismic risk protection?

The methodology has to be explored for real case facilities and it might produce the most value when applied to strategic facilities as hospitals, schools, industrial plants, etc.

On the other hand it would be interesting the comparison of existing prediction method and exploring possible prediction uncertainty mitigation strategies.

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